

Inversor de Voltaje Trifásico

Problema Estudiar el inversor de voltaje con Modulación SPWM.

La moduladora es, $M := 0.9 \quad \omega_s := 2 \cdot \pi \cdot 50 \quad f_M := 0$

$$m_a(t, M) := M \cdot \sin\left(\omega_s \cdot t + f_M - \frac{0 \cdot \pi}{3}\right)$$

$$m_b(t, M) := M \cdot \sin\left(\omega_s \cdot t + f_M - \frac{2 \cdot \pi}{3}\right)$$

$$m_c(t, M) := M \cdot \sin\left(\omega_s \cdot t + f_M - \frac{4 \cdot \pi}{3}\right)$$

La triangular es, $f_{n_tr} := 15 \text{ per} := 1$

$$tri(t) := \frac{2}{\pi} \cdot \text{asin}\left(\sin\left(f_{n_tr} \cdot \omega_s \cdot t + f_M \cdot f_{n_tr} - \pi\right)\right)$$

Las conmutaciones,

$$s_1(t) := \text{if}\left(m_a(t, M) > tri(t), 1, 0\right)$$

$$s_4(t) := \text{if}\left(m_a(t, M) > tri(t), 0, 1\right)$$

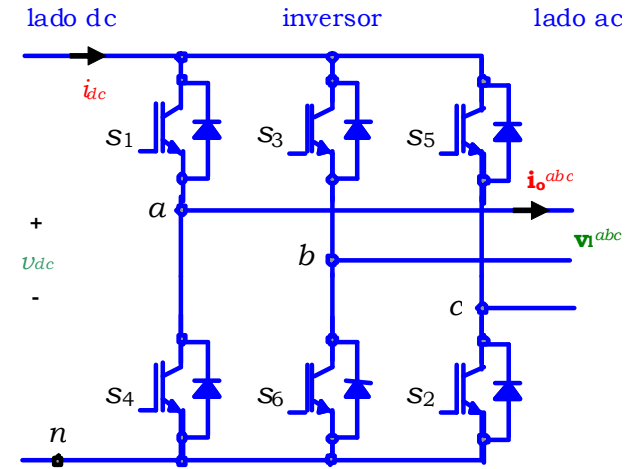
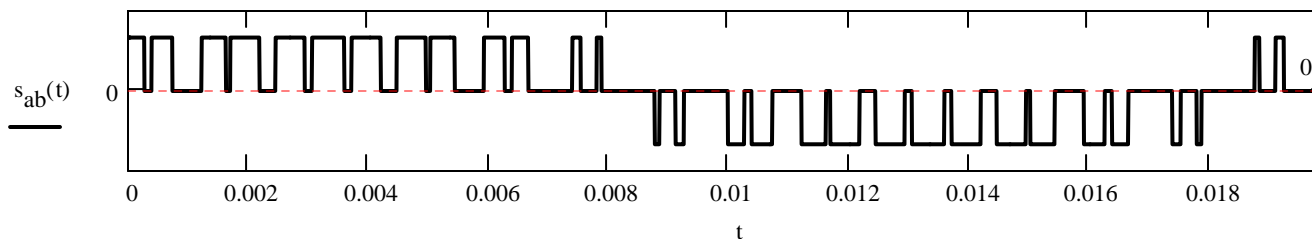
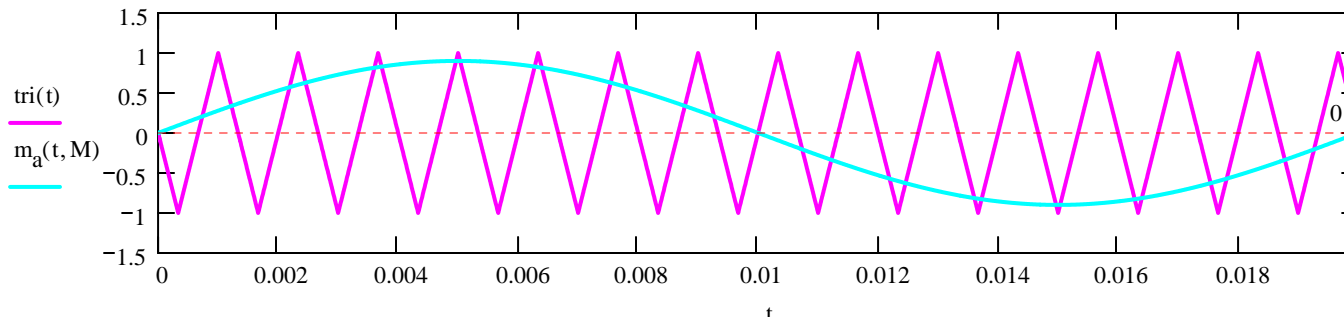
$$s_3(t) := \text{if}\left(m_b(t, M) > tri(t), 1, 0\right)$$

$$s_6(t) := \text{if}\left(m_b(t, M) > tri(t), 0, 1\right)$$

$$s_5(t) := \text{if}\left(m_c(t, M) > tri(t), 1, 0\right)$$

$$s_2(t) := \text{if}\left(m_c(t, M) > tri(t), 0, 1\right)$$

$n_f := f_{n_tr} \cdot 4 \cdot 50 \cdot \text{per} \quad n := 0 \dots n_f \quad t_f := .02 \cdot \text{per} \quad t := 0, \frac{t_f}{n_f} \dots t_f$



Los voltajes se pueden escribir como,

$$v_{an}(t) = s_1(t) \cdot v_{dc}(t) \quad v_{bn}(t) = s_3(t) \cdot v_{dc}(t)$$

$$v_{L_ab}(t) = v_{an}(t) - v_{bn}(t)$$

$$v_{L_ab}(t) = s_1(t) \cdot v_{dc}(t) - s_3(t) \cdot v_{dc}(t)$$

$$v_{L_ab}(t) = (s_1(t) - s_3(t)) \cdot v_{dc}(t)$$

$$v_{L_ab}(t) = s_{ab}(t) \cdot v_{dc}(t)$$

Se define la función de conmutación como,

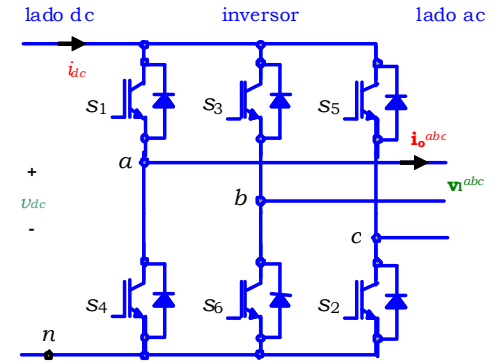
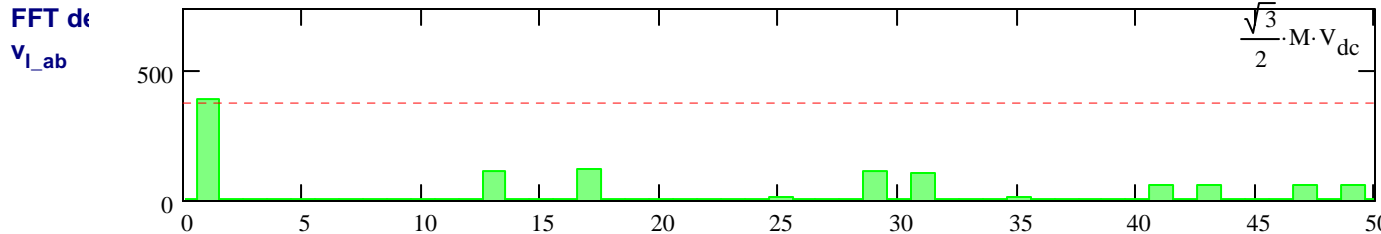
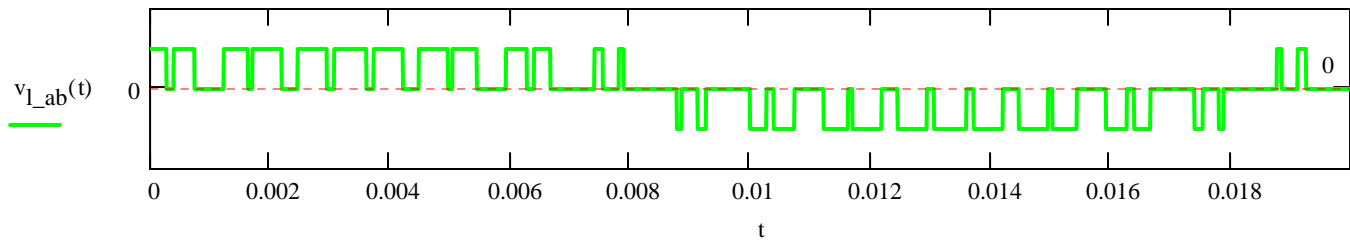
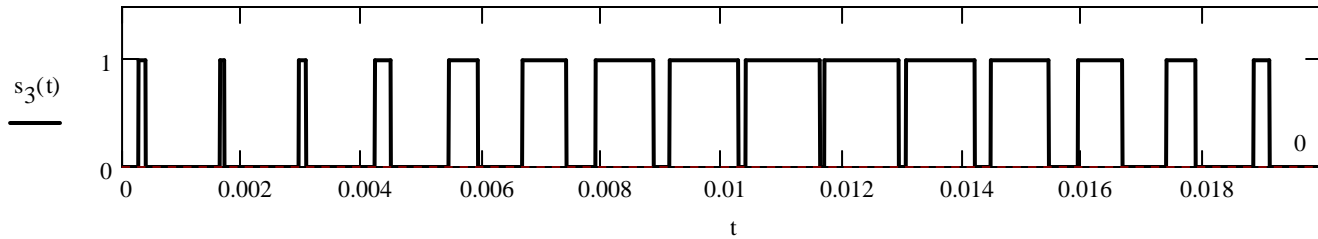
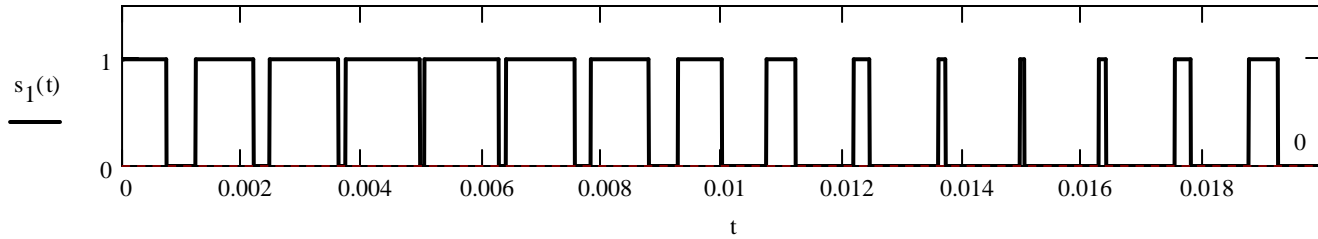
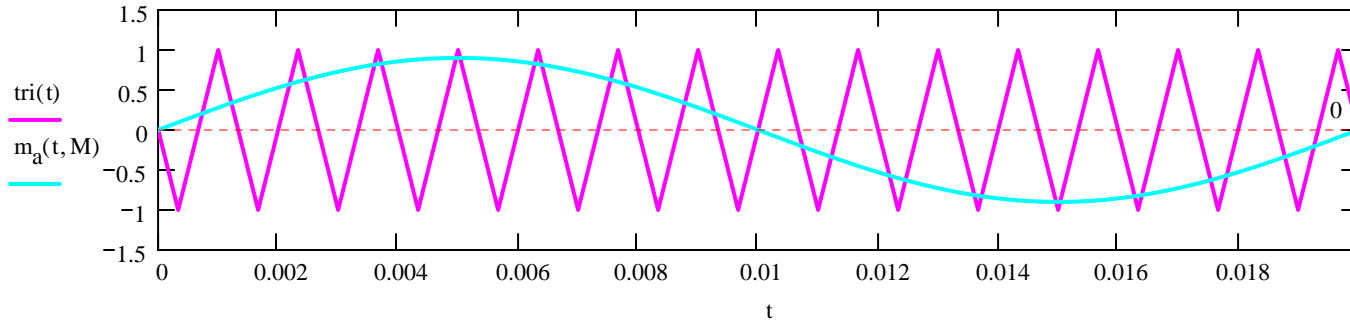
$$s_{ab}(t) := s_1(t) - s_3(t)$$

$$s_{bc}(t) := s_3(t) - s_5(t)$$

$$s_{ca}(t) := s_5(t) - s_1(t)$$

$$v_{L_bc}(t) = s_{bc}(t) \cdot v_{dc}(t)$$

$$v_{L_ca}(t) = s_{ca}(t) \cdot v_{dc}(t)$$



$$s_{ab}(t) := s_1(t) - s_3(t)$$

$$V_{dc} := 500$$

$$v_{dc}(t) := V_{dc}$$

$$v_{l_ab}(t) := s_{ab}(t) \cdot v_{dc}(t)$$

$$N := 1024$$

$$m := 1..N$$

$$x_m := v_{l_ab}\left(\frac{m}{N} \cdot t_f\right)$$

$$xf := \text{FFT}(x)$$

$$xv(m) := \text{if}(m = 1, 1, 2) \cdot x_{m\text{-per}}$$

$$|xv(2)| = 390.691 \cdot \frac{\sqrt{3}}{2} \cdot M \cdot V_{dc} = 389.711$$

La fundamental del voltaje ac es igual a $0.866MV_{dc}$ y no hay componentes de frecuencia hasta $f_{n_tr} / 2$.

Otra Modulación SPWM

$M := 1.05$ $\text{sup}(t) := \text{if}(m_a(t, M) > m_b(t, M), \text{if}(m_a(t, M) > m_c(t, M), m_a(t, M), m_c(t, M)), \text{if}(m_b(t, M) > m_c(t, M), m_b(t, M), m_c(t, M)))$

$\text{inf}(t) := \text{if}(m_a(t, M) < m_b(t, M), \text{if}(m_a(t, M) < m_c(t, M), m_a(t, M), m_c(t, M)), \text{if}(m_b(t, M) < m_c(t, M), m_b(t, M), m_c(t, M)))$ $q_0(t) := (\text{sup}(t) + \text{inf}(t)) \cdot \frac{1}{3} \text{ deC} - \text{DIE}$

$m_{a0}(t, M) := m_a(t, M) - \text{seq}_0(t)$

$m_{b0}(t, M) := m_b(t, M) - \text{seq}_0(t)$

$m_{c0}(t, M) := m_c(t, M) - \text{seq}_0(t)$

$s_1(t) := \text{if}(m_{a0}(t, M) > \text{tri}(t), 1, 0)$

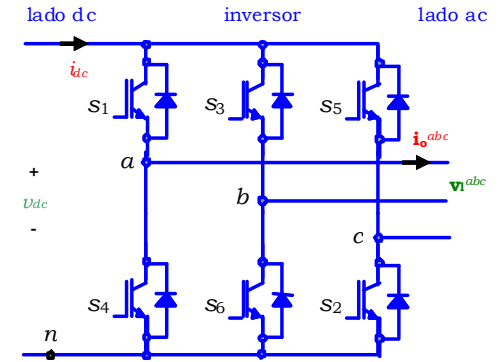
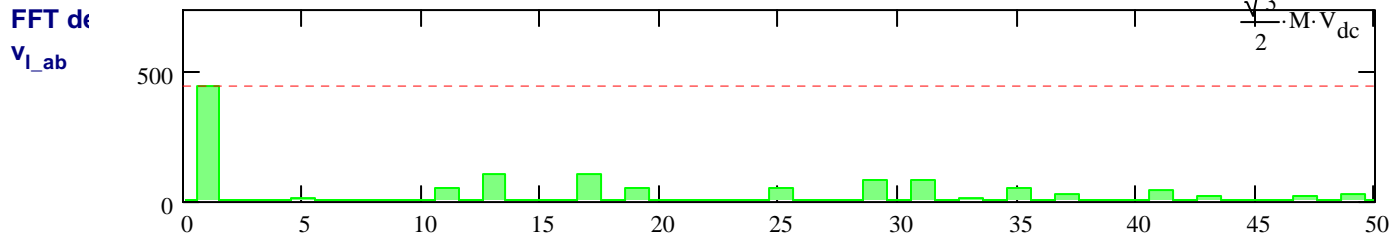
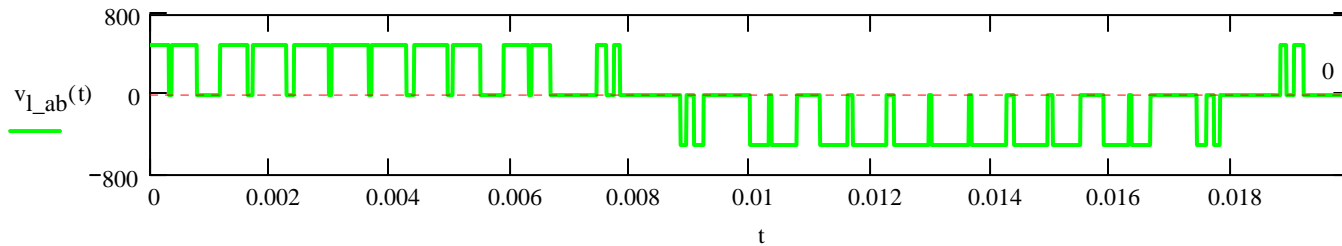
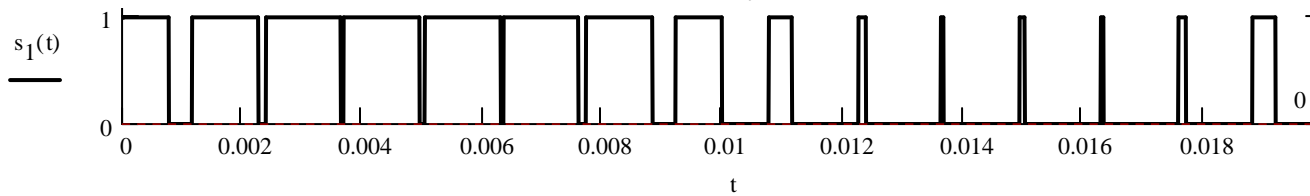
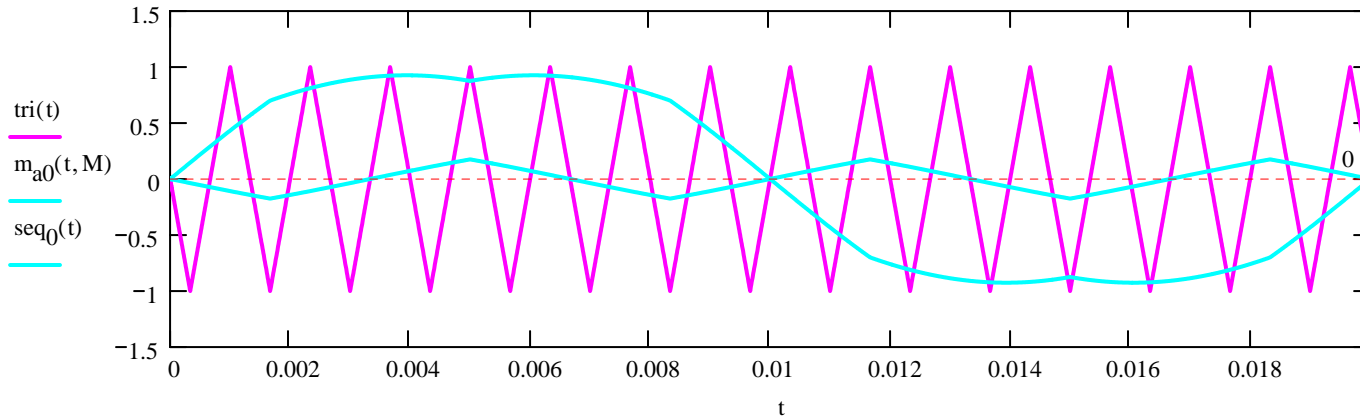
$s_3(t) := \text{if}(m_{b0}(t, M) > \text{tri}(t), 1, 0)$

$s_5(t) := \text{if}(m_{c0}(t, M) > \text{tri}(t), 1, 0)$

$s_{ab}(t) := s_1(t) - s_3(t)$

$s_{bc}(t) := s_3(t) - s_5(t)$

$s_{ca}(t) := s_5(t) - s_1(t)$



$v_{L_ab}(t) := s_{ab}(t) \cdot v_{dc}(t)$

$N := 1024$ $m := 1 \dots N$

$x_m := v_{L_ab}\left(\frac{m}{N} \cdot t_f\right)$ $xf := \text{FFT}(x)$

$xv(m) := \text{if}(m = 1, 1, 2) \cdot xf_{m_per}$

$|xv(2)| = 450.01$ $\frac{\sqrt{3}}{2} \cdot M \cdot V_{dc} = 454.663$

La fundamental del voltaje ac es igual a $0.866MV_{dc}$ y no hay componentes de frecuencia hasta $f_{n_tr} / 2$. M puede llegar a ser 1.17

Modelo de Inversor de Voltaje Trifásico

Problema Estudiar el modelo del inversor de voltaje con Modulación SPWM.

La suma de las corrientes de carga es cero y la carga es balanceada, entonces,

$$v_{o_an}(t) + v_{o_bn}(t) + v_{o_cn}(t) = 0$$

por lo tanto,

$$\begin{pmatrix} v_{l_ab}(t) \\ v_{l_bc}(t) \\ 0 \end{pmatrix} = \begin{pmatrix} 1 & -1 & 0 \\ 0 & 1 & -1 \\ 1 & 1 & 1 \end{pmatrix} \cdot \begin{pmatrix} v_{o_an}(t) \\ v_{o_bn}(t) \\ v_{o_cn}(t) \end{pmatrix}$$

$$v_{l_ab}(t) = s_{ab}(t) \cdot v_{dc}(t) = (s_1(t) - s_3(t)) \cdot v_{dc}(t)$$

$$v_{l_bc}(t) = s_{bc}(t) \cdot v_{dc}(t) = (s_3(t) - s_5(t)) \cdot v_{dc}(t)$$

$$v_{l_ca}(t) = s_{ca}(t) \cdot v_{dc}(t) = (s_5(t) - s_1(t)) \cdot v_{dc}(t)$$

$$\begin{pmatrix} v_{o_an}(t) \\ v_{o_bn}(t) \\ v_{o_cn}(t) \end{pmatrix} = \frac{1}{3} \cdot \begin{pmatrix} 2 & 1 & 1 \\ -1 & 1 & 1 \\ -1 & -2 & 1 \end{pmatrix} \cdot \begin{pmatrix} v_{l_ab}(t) \\ v_{l_bc}(t) \\ 0 \end{pmatrix}$$

$$\begin{pmatrix} v_{o_an}(t) \\ v_{o_bn}(t) \\ v_{o_cn}(t) \end{pmatrix} = \frac{1}{3} \cdot \begin{pmatrix} 2 & 1 & 1 \\ -1 & 1 & 1 \\ -1 & -2 & 1 \end{pmatrix} \cdot \begin{pmatrix} 1 & -1 & 0 \\ 0 & 1 & -1 \\ 0 & 0 & 0 \end{pmatrix} \cdot \begin{pmatrix} s_1(t) \\ s_3(t) \\ s_5(t) \end{pmatrix} \cdot v_{dc}(t) = \frac{1}{3} \cdot \begin{pmatrix} 2 & -1 & -1 \\ -1 & 2 & -1 \\ -1 & -1 & 2 \end{pmatrix} \cdot \begin{pmatrix} s_1(t) \\ s_3(t) \\ s_5(t) \end{pmatrix} \cdot v_{dc}(t)$$

$$v_{o_an}(t) = R_o \cdot i_{o_a}(t) + L_o \cdot di_{o_a}(t)$$

$$v_{o_bn}(t) = R_o \cdot i_{o_b}(t) + L_o \cdot di_{o_b}(t)$$

$$v_{o_cn}(t) = R_o \cdot i_{o_c}(t) + L_o \cdot di_{o_c}(t)$$

$$v_{dc}(t) \cdot i_{dc}(t) = v_{o_n}(t)^T \cdot i_o(t)$$

$$v_{o_n}(t) = T_{In} \cdot s_i(t) \cdot v_{dc}(t)$$

$$v_{dc}(t) \cdot i_{dc}(t) = (T_{In} \cdot s_i(t) \cdot v_{dc}(t))^T \cdot i_o(t)$$

$$i_{dc}(t) = s_i(t)^T \cdot T_{In}^T \cdot i_o(t)$$

$$i_{dc}(t) = s_i(t)^T \cdot T_{In} \cdot i_o(t)$$

$$T_{In} := \frac{1}{3} \cdot \begin{pmatrix} 2 & -1 & -1 \\ -1 & 2 & -1 \\ -1 & -1 & 2 \end{pmatrix} \quad T_{In}^T = T_{In}$$

$$s_i(t) := \begin{pmatrix} s_1(t) \\ s_3(t) \\ s_5(t) \end{pmatrix}$$

$$T_{In} \cdot s_i(t) \cdot v_{dc}(t) = R_o \cdot i_o(t) + L_o \cdot di_o(t)$$

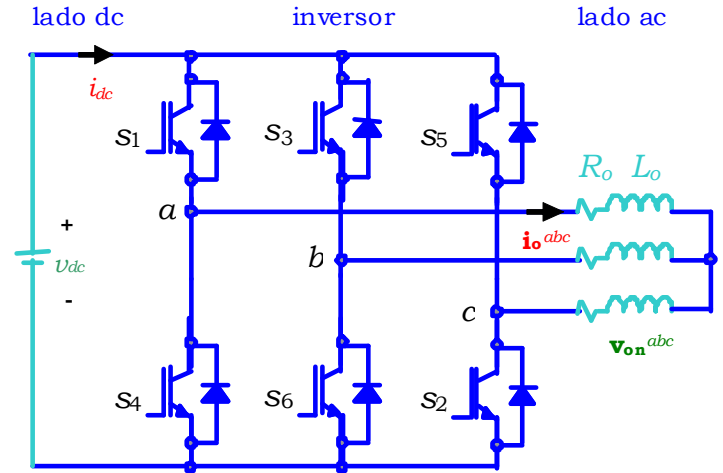
$$di_o(t) = \frac{-R_o}{L_o} \cdot i_o(t) + \frac{1}{L_o} \cdot T_{In} \cdot s_i(t) \cdot v_{dc}(t)$$

Parámetros

$$L_o := 15 \cdot 10^{-3}$$

$$R_o := 10$$

$$v_{dc}(t) := V_{dc}$$



Simulación $t_f := 0.02$ $n_f := 2048$ $n := 1 .. n_f$ $t := 0, \frac{t_f}{n_f} .. t_f$

$$D(t, x) := \frac{-R_o}{L_o} \cdot (x_1 \ x_2 \ x_3)^T + \frac{1}{L_o} \cdot T_{In} \cdot s_i(t) \cdot v_{dc}(t) \quad CI := \begin{pmatrix} 0 \\ 0 \\ 0 \end{pmatrix} \quad Z := \text{rkfixed}(CI, 0, t_f, n_f, D) \quad CI := \left(Z_{n_f, 2} \ Z_{n_f, 3} \ Z_{n_f, 4} \right)^T \quad Z := \text{rkfixed}(CI, 0, t_f, n_f, D)$$

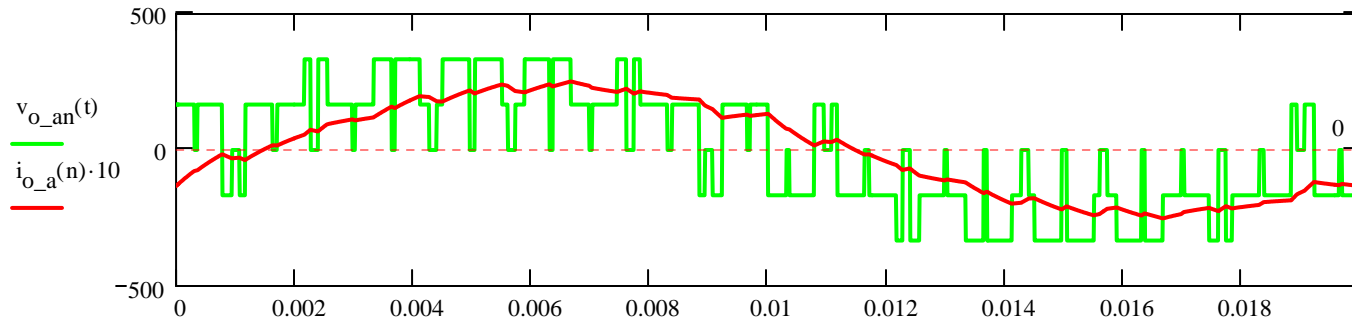
$$v_{o_an}(t) := \left(T_{ln} \cdot s_i(t) \cdot v_{dc}(t) \right)_1 \quad v_{o_bn}(t) := \left(T_{ln} \cdot s_i(t) \cdot v_{dc}(t) \right)_2 \quad v_{o_cn}(t) := \left(T_{ln} \cdot s_i(t) \cdot v_{dc}(t) \right)_3$$

$$i_{o_a}(n) := Z_{n,2}$$

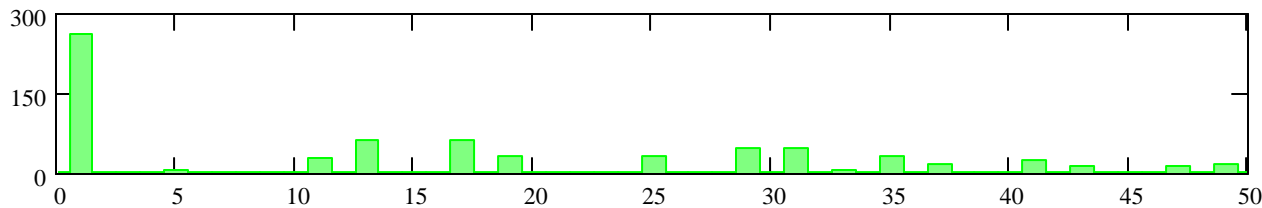
$$i_{o_b}(n) := Z_{n,3}$$

$$i_{o_c}(n) := Z_{n,4}$$

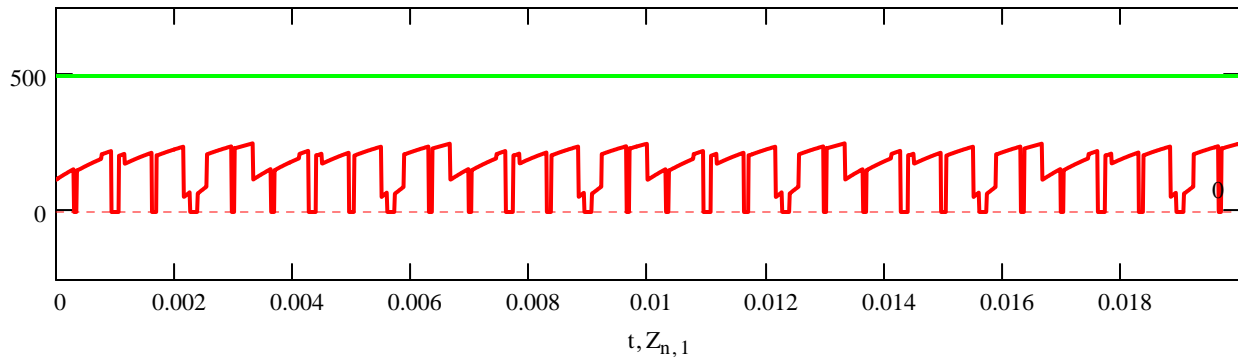
$$i_{dc}(n) := \left(s_i \left(n \cdot \frac{t_f}{n_f} \right) \right)^T \cdot (T_{ln})^T \cdot (i_{o_a}(n) \ i_{o_b}(n) \ i_{o_c}(n))^T \quad \text{UdeC - DIE}$$



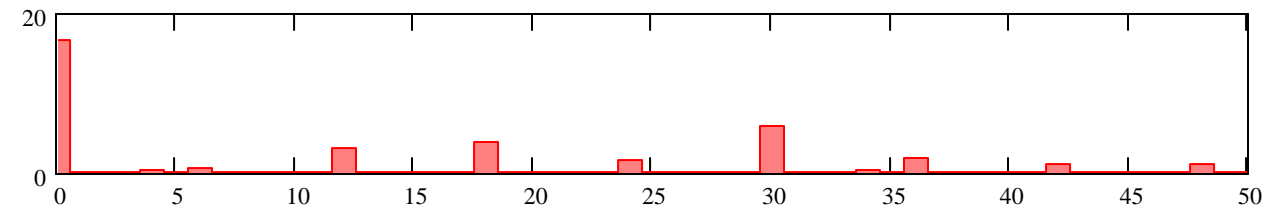
FFT de v_{o_an}



FFT de i_{dc}



FFT de i_{dc}



$$N := 1024 \quad m := 1..N$$

$$x_m := v_{o_an} \left(\frac{m}{N} \cdot t_f \right) \quad xf := \text{FFT}(x)$$

$$xv(m) := \text{if}(m = 1, 1, 2) \cdot xf_{m_per}$$

$$|xv(2)| = 259.337 \quad V_{o_n_rms} := \frac{1}{2} \cdot M \cdot \frac{V_{dc}}{\sqrt{2}}$$

$$v_{o_an1}(t) = \frac{V_{dc}}{2} \cdot m_a(t) \quad f \leq \frac{f_{n_tr}}{2}$$

La fundamental de voltaje de carga es igual a la moduladora sobre 2.

$$I_{o_rms} := \frac{1}{2} \cdot M \cdot \frac{V_{dc}}{\sqrt{2}} \cdot \frac{1}{\sqrt{R_o^2 + (\omega_s \cdot L_o)^2}}$$

$$N := 1024 \quad m := 1..N$$

$$x_m := i_{dc} \left(\frac{m}{N} \cdot n_f \right) \quad xf := \text{FFT}(x)$$

$$xv(m) := \text{if}(m = 1, 1, 2) \cdot xf_{m_per}$$

$$|xv(1)| = 16.653$$

$$P_o := 3 \cdot V_{o_n_rms} \cdot I_{o_rms} \cdot \cos \left(\text{atan} \left(\omega_s \cdot \frac{L_o}{R_o} \right) \right)$$

$$I_{dc} := \frac{P_o}{V_{dc}} \quad I_{dc} = 16.916$$

La corriente DC no tiene segunda armónica. Sólo armónicas de conmutación.

Modelo Promedio de Inversor de Voltaje Monofásico

Problema Estudiar el modelo promedio del inversor de voltaje.

Se opta por trabajar con la fundamental.

Como la suma de las corrientes de carga es cero y la carga es balanceada, entonces,

$$v_{o_an}(t) + v_{o_bn}(t) + v_{o_cn}(t) = 0$$

por lo tanto,

$$\begin{pmatrix} v_{l_ab}(t) \\ v_{l_bc}(t) \\ v_{l_ca}(t) \end{pmatrix} = \begin{pmatrix} 1 & -1 & 0 \\ 0 & 1 & -1 \\ -1 & 0 & 1 \end{pmatrix} \cdot \begin{pmatrix} v_{o_an}(t) \\ v_{o_bn}(t) \\ v_{o_cn}(t) \end{pmatrix} = \frac{1}{2} \cdot \begin{pmatrix} 1 & -1 & 0 \\ 0 & 1 & -1 \\ -1 & 0 & 1 \end{pmatrix} \cdot \begin{pmatrix} m_a(t) \\ m_b(t) \\ m_c(t) \end{pmatrix} \cdot v_{dc}(t)$$

$$\begin{pmatrix} v_{l_ab}(t) \\ v_{l_bc}(t) \\ v_{l_ca}(t) \end{pmatrix} = \frac{1}{2} \cdot \begin{pmatrix} m_a(t) - m_b(t) \\ m_b(t) - m_c(t) \\ m_c(t) - m_a(t) \end{pmatrix} \cdot v_{dc}(t) = \begin{pmatrix} m_{ab}(t) \\ m_{bc}(t) \\ m_{ca}(t) \end{pmatrix} \cdot v_{dc}(t)$$

$$v_{o_an}(t) = R_o \cdot i_{o_a}(t) + L_o \cdot di_{o_a}(t)$$

$$v_{o_bn}(t) = R_o \cdot i_{o_b}(t) + L_o \cdot di_{o_b}(t)$$

$$v_{o_cn}(t) = R_o \cdot i_{o_c}(t) + L_o \cdot di_{o_c}(t)$$

$$m_i(t) \cdot v_{dc}(t) = R_o \cdot i_o(t) + L_o \cdot di_o(t)$$

$$di_o(t) = \frac{-R_o}{L_o} \cdot i_o(t) + \frac{1}{L_o} \cdot m_i(t) \cdot v_{dc}(t)$$

$$\begin{pmatrix} v_{o_an}(t) \\ v_{o_bn}(t) \\ v_{o_cn}(t) \end{pmatrix} = \frac{1}{2} \cdot \begin{pmatrix} m_a(t) \\ m_b(t) \\ m_c(t) \end{pmatrix} \cdot v_{dc}(t)$$

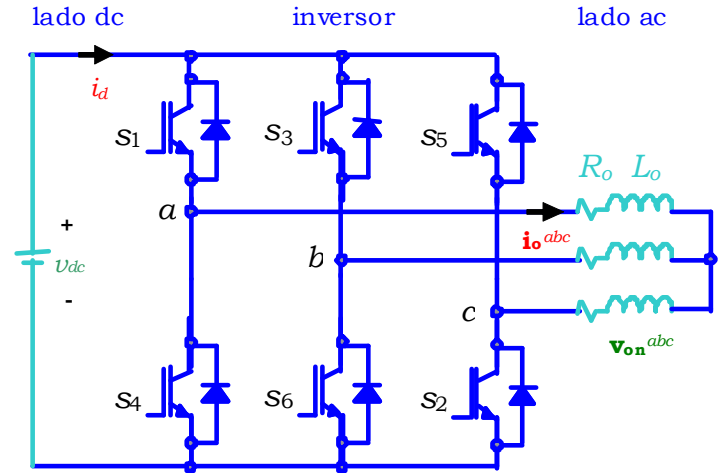
$$v_{dc}(t) \cdot i_{dc}(t) = v_{o_n}(t)^T \cdot i_o(t)$$

$$v_{o_n}(t) = m_i(t) \cdot v_{dc}(t)$$

$$v_{dc}(t) \cdot i_{dc}(t) = (m_i(t) \cdot v_{dc}(t))^T \cdot i_o(t)$$

$$i_{dc}(t) = m_i(t)^T \cdot i_o(t)$$

$$i_{dc}(t) = m_i(t)^T \cdot i_o(t)$$



$$m_i(t) := \frac{1}{2} \cdot \begin{pmatrix} m_a(t, M) \\ m_b(t, M) \\ m_c(t, M) \end{pmatrix}$$

Parámetros

$$L_o := 15 \cdot 10^{-3}$$

$$R_o := 10$$

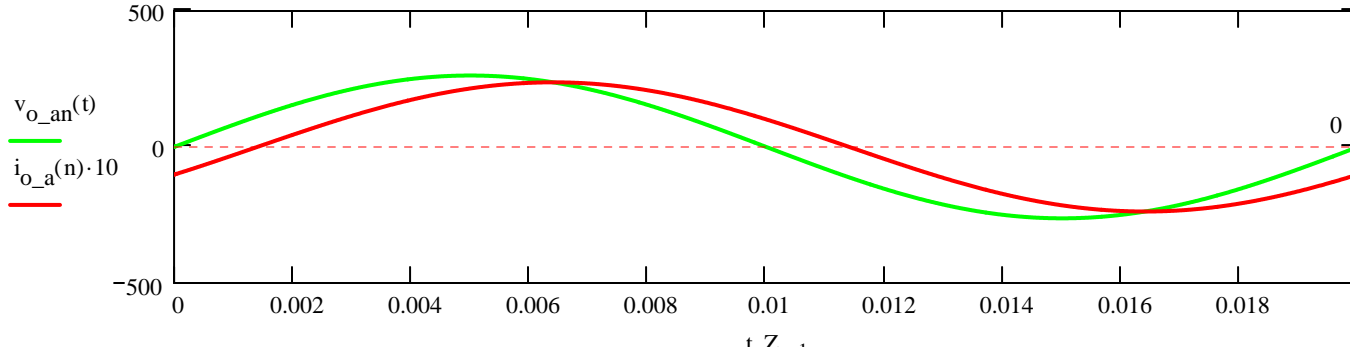
$$v_{dc}(t) := V_{dc}$$

Simulación $t_f := 0.02$ $n_f := 2048$ $n := 1 .. n_f$ $t := 0, \frac{t_f}{n_f} .. t_f$

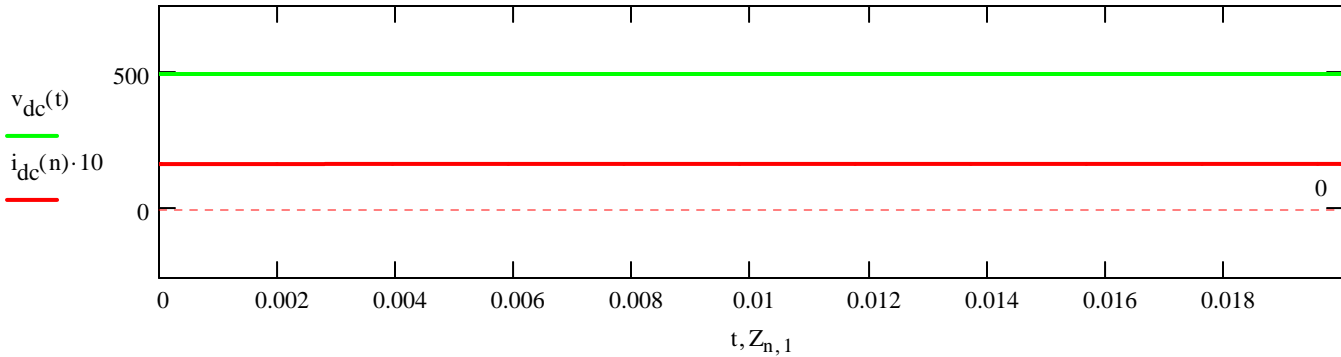
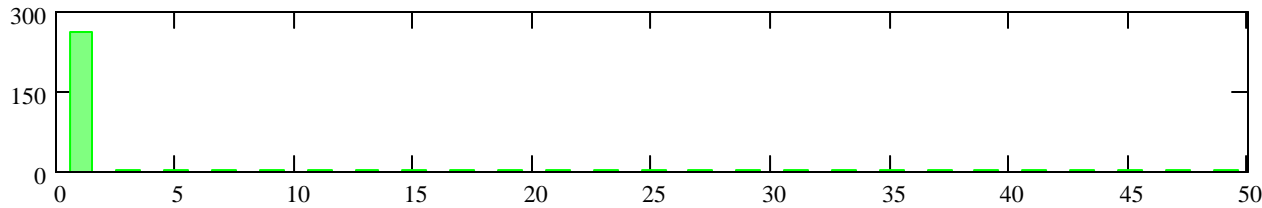
$$D(t, x) := \frac{-R_o}{L_o} \cdot (x_1 \ x_2 \ x_3)^T + \frac{1}{L_o} \cdot m_i(t) \cdot v_{dc}(t) \quad CI := \begin{pmatrix} 0 \\ 0 \\ 0 \end{pmatrix} \quad Z := \text{rkfixed}(CI, 0, t_f, n_f, D) \quad CI := \begin{pmatrix} Z_{n_f, 2} & Z_{n_f, 3} & Z_{n_f, 4} \end{pmatrix}^T \quad Z := \text{rkfixed}(CI, 0, t_f, n_f, D)$$

$$v_{o_an}(t) := (m_i(t) \cdot v_{dc}(t))_1 \quad v_{o_bn}(t) := (m_i(t) \cdot v_{dc}(t))_2 \quad v_{o_cn}(t) := (m_i(t) \cdot v_{dc}(t))_3$$

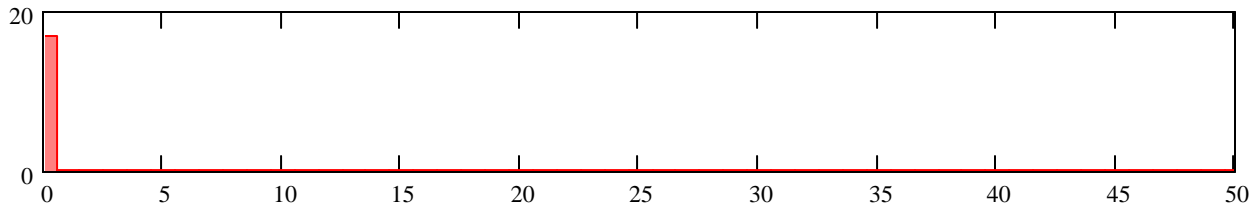
$$i_{o_a}(n) := Z_{n,2} \quad i_{o_b}(n) := Z_{n,3} \quad i_{o_c}(n) := Z_{n,4} \quad i_{dc}(n) := \left(m_i \left(n \cdot \frac{t_f}{n_f} \right) \right)^T \cdot (i_{o_a}(n) \ i_{o_b}(n) \ i_{o_c}(n))^T$$



FFT de v_{o_an}



FFT de i_{dc}



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N := 1024      m := 1..N
x_m := v_o_an(m/N * t_f)  xf := FFT(x)
xv(m) := if(m = 1, 1, 2) * xf_m_per
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$$|xv(2)| = 262.5 \quad V_{o_n_rms} := \frac{1}{2} \cdot M \cdot \frac{V_{dc}}{\sqrt{2}}$$

$$\frac{1}{2} \cdot M \cdot V_{dc} = 262.5$$

La fundamental de voltaje de carga es igual a la moduladora sobre 2.

$$I_{o_rms} := \frac{1}{2} \cdot M \cdot \frac{V_{dc}}{\sqrt{2}} \cdot \frac{1}{\sqrt{R_o^2 + (\omega_s \cdot L_o)^2}}$$

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N := 1024      m := 1..N
x_m := i_dc(m/N * n_f)  xf := FFT(x)
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$$|xv(1)| = 16.888$$

$$P_o := 3 \cdot V_{o_n_rms} \cdot I_{o_rms} \cdot \cos\left(\text{atan}\left(\omega_s \cdot \frac{L_o}{R_o}\right)\right)$$

$$I_{dc} := \frac{P_o}{V_{dc}} \quad I_{dc} = 16.916$$

La corriente DC no tiene segunda armónica.

Modelo de Rectificador de Voltaje Trifásico

Problema Estudiar el modelo del rectificador de voltaje con Modulación SPWM.

$$v_{r_an}(t) + v_{r_bn}(t) + v_{r_cn}(t) = 0$$

$$\begin{pmatrix} v_{r_ab}(t) \\ v_{r_bc}(t) \\ 0 \end{pmatrix} = \begin{pmatrix} 1 & -1 & 0 \\ 0 & 1 & -1 \\ 1 & 1 & 1 \end{pmatrix} \cdot \begin{pmatrix} v_{r_an}(t) \\ v_{r_bn}(t) \\ v_{r_cn}(t) \end{pmatrix}$$

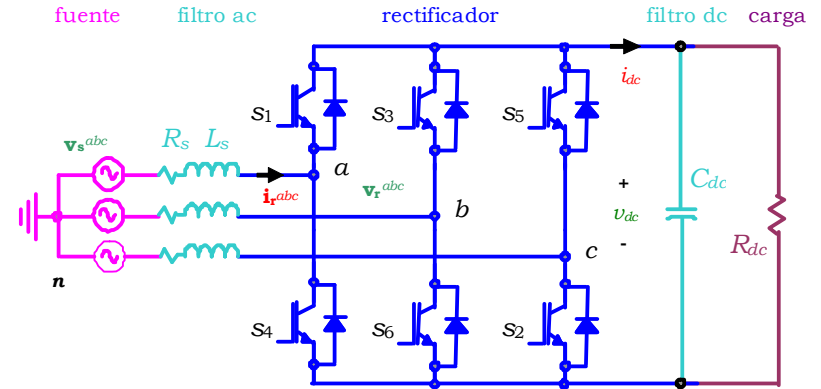
$$v_{r_ab}(t) = s_{ab}(t) \cdot v_{dc}(t) = (s_1(t) - s_3(t)) \cdot v_{dc}(t)$$

$$v_{r_bc}(t) = s_{bc}(t) \cdot v_{dc}(t) = (s_3(t) - s_5(t)) \cdot v_{dc}(t)$$

$$v_{r_ca}(t) = s_{ca}(t) \cdot v_{dc}(t) = (s_5(t) - s_1(t)) \cdot v_{dc}(t)$$

Parámetros

$$\begin{matrix} L_s := 30 \cdot 10^{-3} & R_s := 1 \\ C_{dc} := 500 \cdot 10^{-6} & R_{dc} := 100 \end{matrix}$$



$$\begin{pmatrix} v_{r_an}(t) \\ v_{r_bn}(t) \\ v_{r_cn}(t) \end{pmatrix} = \frac{1}{3} \cdot \begin{pmatrix} 2 & -1 & -1 \\ -1 & 1 & 1 \\ -1 & -2 & 1 \end{pmatrix} \cdot \begin{pmatrix} v_{r_ab}(t) \\ v_{r_bc}(t) \\ 0 \end{pmatrix} = \frac{1}{3} \cdot \begin{pmatrix} 2 & -1 & -1 \\ -1 & 1 & 1 \\ -1 & -2 & 1 \end{pmatrix} \cdot \begin{pmatrix} 1 & -1 & 0 \\ 0 & 1 & -1 \\ 0 & 0 & 0 \end{pmatrix} \cdot \begin{pmatrix} s_1(t) \\ s_3(t) \\ s_5(t) \end{pmatrix} \cdot v_{dc}(t) = \frac{1}{3} \cdot \begin{pmatrix} 2 & -1 & -1 \\ -1 & 2 & -1 \\ -1 & -1 & 2 \end{pmatrix} \cdot \begin{pmatrix} s_1(t) \\ s_3(t) \\ s_5(t) \end{pmatrix} \cdot v_{dc}(t) = T_{ln} \cdot s_r(t) \cdot v_{dc}(t)$$

$$v_{s_a}(t) = R_s \cdot i_{r_a}(t) + L_s \cdot di_{r_a}(t) + v_{r_an}(t)$$

$$v_{s_b}(t) = R_s \cdot i_{r_b}(t) + L_s \cdot di_{r_b}(t) + v_{r_bn}(t)$$

$$v_{s_c}(t) = R_s \cdot i_{r_c}(t) + L_s \cdot di_{r_c}(t) + v_{r_cn}(t)$$

$$i_{dc}(t) = C_{dc} \cdot dv_{dc}(t) + \frac{v_{dc}(t)}{R_{dc}}$$

$$v_{dc}(t) \cdot i_{dc}(t) = v_{r_n}(t) \cdot i_r(t)$$

$$v_{r_n}(t) = T_{ln} \cdot s_r(t) \cdot v_{dc}(t)$$

$$v_{dc}(t) \cdot i_{dc}(t) = (T_{ln} \cdot s_r(t) \cdot v_{dc}(t))^T \cdot i_r(t)$$

$$i_{dc}(t) = s_r(t)^T \cdot T_{ln} \cdot i_r(t)$$

$$i_{dc}(t) = s_r(t)^T \cdot T_{ln} \cdot i_r(t)$$

$$v_s(t) = R_s \cdot i_r(t) + L_s \cdot di_r(t) + T_{ln} \cdot s_r(t) \cdot v_{dc}(t)$$

$$s_r(t)^T \cdot T_{ln} \cdot i_r(t) = C_{dc} \cdot dv_{dc}(t) + \frac{v_{dc}(t)}{R_{dc}}$$

$$di_r(t) = \frac{-R_s}{L_s} \cdot i_r(t) - \frac{1}{L_s} \cdot T_{ln} \cdot s_r(t) \cdot v_{dc}(t) + \frac{1}{L_s} \cdot v_s(t)$$

$$dv_{dc}(t) = \frac{-1}{C_{dc} \cdot R_{dc}} \cdot v_{dc}(t) + \frac{1}{C_{dc}} \cdot s_r(t)^T \cdot T_{ln} \cdot i_r(t)$$

$$s_r(t) := s_i(t)$$

$$v_s(t) := \left(\sqrt{2} \cdot 220 \cdot \sin(\omega_s \cdot t) \quad \sqrt{2} \cdot 220 \cdot \sin\left(\omega_s \cdot t - 2 \cdot \frac{\pi}{3}\right) \quad \sqrt{2} \cdot 220 \cdot \sin\left(\omega_s \cdot t - 4 \cdot \frac{\pi}{3}\right) \right)^T$$

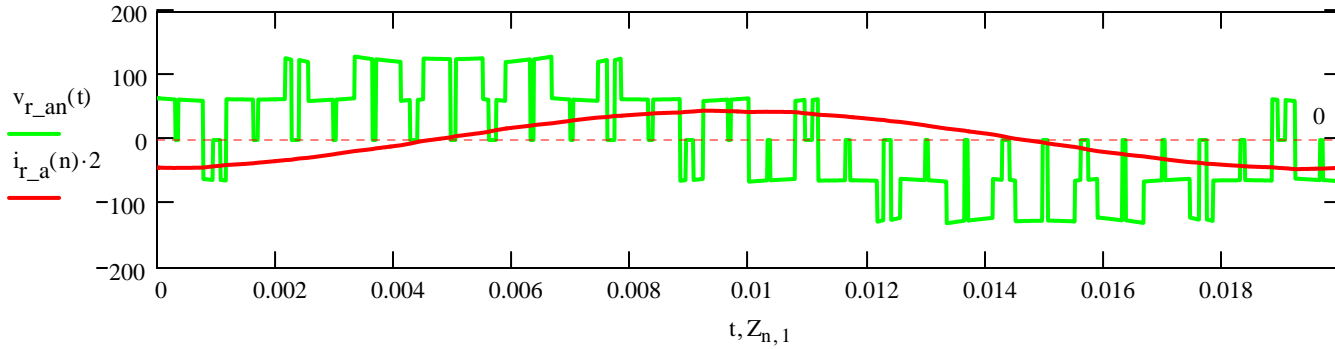
Simulación $t_f := 0.02$ $n_f := 2048$ $n := 1 \dots n_f$ $t := 0, \frac{t_f}{n_f} \dots t_f$

$$D(t, x) := \text{stack} \left(\frac{-R_s}{L_s} \cdot (x_1 \ x_2 \ x_3)^T - \frac{1}{L_s} \cdot T_{ln} \cdot s_r(t) \cdot x_4 + \frac{1}{L_s} \cdot v_s(t), \frac{-1}{C_{dc} \cdot R_{dc}} \cdot x_4 + \frac{1}{C_{dc}} \cdot (s_r(t))^T \cdot T_{ln} \cdot (x_1 \ x_2 \ x_3)^T \right)$$

$$CI := (-21.463 \ 8.749 \ 12.714 \ 197.244)^T \quad Z := \text{rkfixed}(CI, 0, t_f, n_f, D) \quad CI := (Z_{n_f,2} \ Z_{n_f,3} \ Z_{n_f,4} \ Z_{n_f,5})^T \quad Z := \text{rkfixed}(CI, 0, t_f, n_f, D)$$

$$v_{dc}(n) := Z_{n,5} \quad v_{r_an}(t) := \left(T_{ln} \cdot s_r(t) \cdot v_{dc} \left(t \cdot \frac{n_f}{t_f} \right) \right)_1 \quad v_{r_bn}(t) := \left(T_{ln} \cdot s_r(t) \cdot v_{dc} \left(t \cdot \frac{n_f}{t_f} \right) \right)_2 \quad v_{r_cn}(t) := \left(T_{ln} \cdot s_r(t) \cdot v_{dc} \left(t \cdot \frac{n_f}{t_f} \right) \right)_3$$

$$i_{r_a}(n) := Z_{n,2} \quad i_{r_b}(n) := Z_{n,3} \quad i_{r_c}(n) := Z_{n,4} \quad i_{dc}(n) := \left(s_r \left(n \cdot \frac{t_f}{n_f} \right) \right)^T \cdot (T_{ln})^T \cdot (i_{r_a}(n) \ i_{r_b}(n) \ i_{r_c}(n))^T$$



N := 1024 m := 1..N

$x_m := v_{r_an} \left(\frac{m}{N} \cdot t_f \right)$ xf := FFT(x)

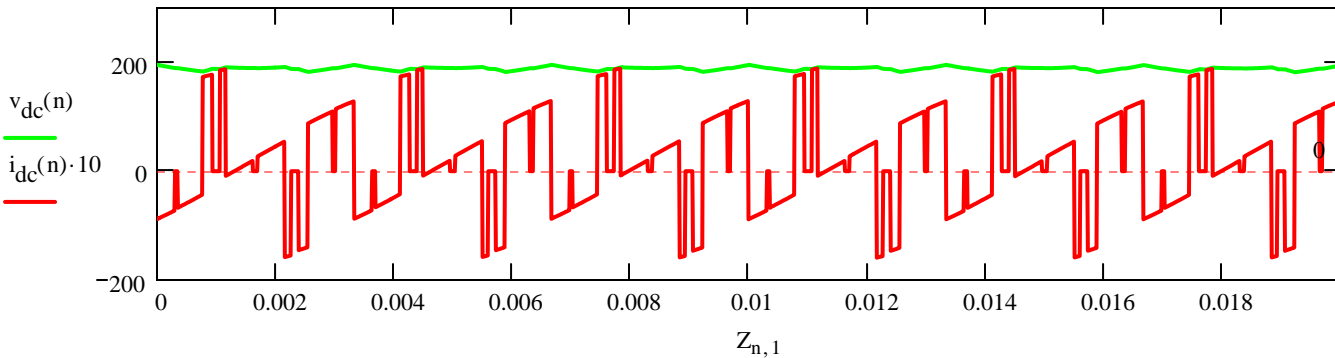
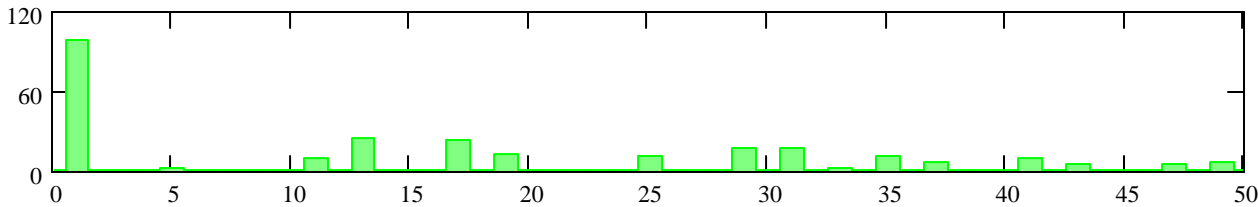
xv(m) := if(m = 1, 1, 2) * xf_m_per

|xv(2)| = 97.834

$\frac{1}{2} \cdot M \cdot v_{dc}(1) = 102.624$

La fundamental de voltaje de fase es igual a la moduladora sobre 2.

FFT de v_{r_an}



N := 1024 m := 1..N

$x_m := i_{dc} \left(\frac{m}{N} \cdot n_f \right)$ xf := FFT(x)

xv(m) := if(m = 1, 1, 2) * xf_m_per

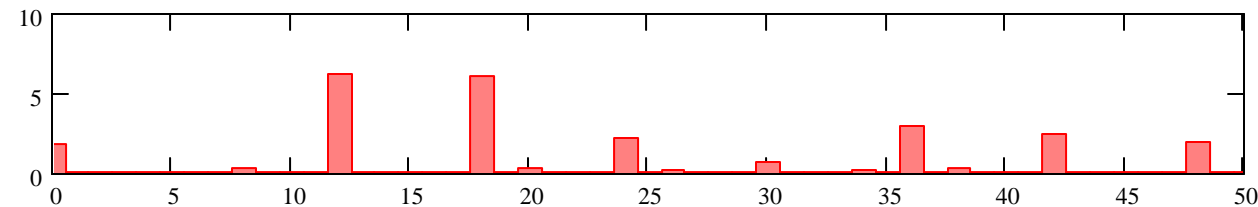
|xv(1)| = 1.814 I_dc := |xv(1)|

$P_o := R_{dc} \cdot I_{dc}^2$

$P_o = 329.069$

La corriente DC no tiene segunda armónica. Sólo armónicas de conmutación.

FFT de i_{dc}



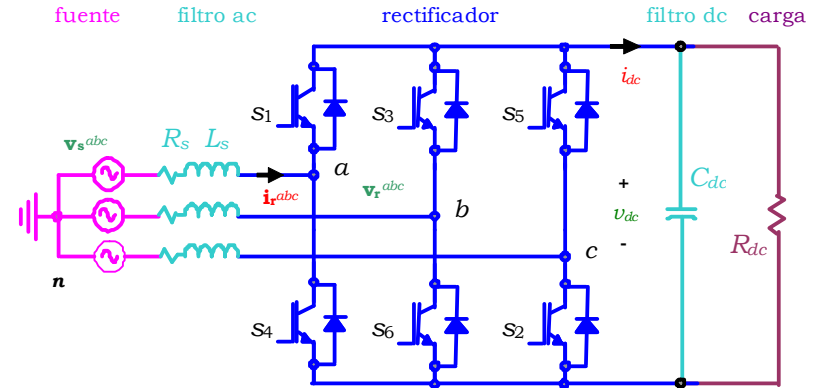
Modelo Promedio de Rectificador de Voltaje Trifásico

Problema Estudiar el modelo promedio del rectificador de voltaje.

$$\begin{pmatrix} v_{r_an}(t) \\ v_{r_bn}(t) \\ v_{r_cn}(t) \end{pmatrix} = m_r(t) \cdot v_{dc}(t)$$

Parámetros

$$\begin{aligned} L_s &:= 30 \cdot 10^{-3} & R_s &:= 1 \\ C_{dc} &:= 500 \cdot 10^{-6} & R_{dc} &:= 100 \end{aligned}$$



$$v_{s_a}(t) = R_s \cdot i_{r_a}(t) + L_s \cdot di_{r_a}(t) + v_{r_an}(t)$$

$$v_{s_b}(t) = R_s \cdot i_{r_b}(t) + L_s \cdot di_{r_b}(t) + v_{r_bn}(t)$$

$$v_{s_c}(t) = R_s \cdot i_{r_c}(t) + L_s \cdot di_{r_c}(t) + v_{r_cn}(t)$$

$$i_{dc}(t) = C_{dc} \cdot dv_{dc}(t) + \frac{v_{dc}(t)}{R_{dc}}$$

$$v_{dc}(t) \cdot i_{dc}(t) = v_{r_n}(t)^T \cdot i_r(t)$$

$$v_{r_n}(t) = m_r(t) \cdot v_{dc}(t)$$

$$v_{dc}(t) \cdot i_{dc}(t) = (m_r(t) \cdot v_{dc}(t))^T \cdot i_r(t)$$

$$i_{dc}(t) = m_r(t)^T \cdot i_r(t)$$

$$i_{dc}(t) = m_r(t)^T \cdot i_r(t)$$

$$v_s(t) = R_s \cdot i_r(t) + L_s \cdot di_r(t) + m_r(t) \cdot v_{dc}(t)$$

$$m_r(t)^T \cdot i_r(t) = C_{dc} \cdot dv_{dc}(t) + \frac{v_{dc}(t)}{R_{dc}}$$

$$di_r(t) = \frac{-R_s}{L_s} \cdot i_r(t) - \frac{1}{L_s} \cdot m_r(t) \cdot v_{dc}(t) + \frac{1}{L_s} \cdot v_s(t)$$

$$dv_{dc}(t) = \frac{-1}{C_{dc} \cdot R_{dc}} \cdot v_{dc}(t) + \frac{1}{C_{dc}} \cdot m_r(t)^T \cdot i_r(t)$$

$$v_s(t) := \begin{pmatrix} \sqrt{2} \cdot 220 \cdot \sin(\omega_s \cdot t) & \sqrt{2} \cdot 220 \cdot \sin(\omega_s \cdot t - 2 \cdot \frac{\pi}{3}) & \sqrt{2} \cdot 220 \cdot \sin(\omega_s \cdot t - 4 \cdot \frac{\pi}{3}) \end{pmatrix}^T$$

Simulación $t_f := 0.02$ $n_f := 2048$ $n := 1 .. n_f$ $t := 0, \frac{t_f}{n_f} .. t_f$

$$m_r(t) := m_1(t)$$

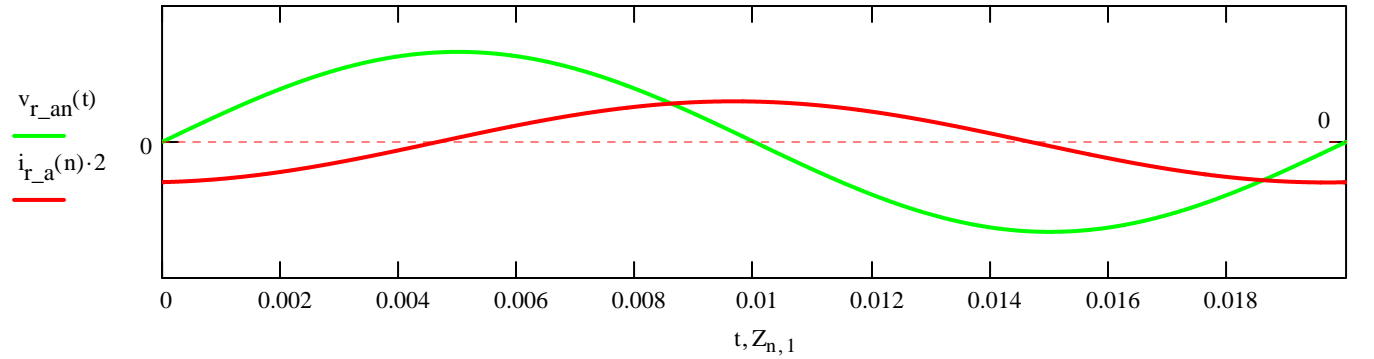
$$D(t, x) := \text{stack} \left(\frac{-R_s}{L_s} \cdot (x_1 \ x_2 \ x_3)^T - \frac{1}{L_s} \cdot m_r(t) \cdot x_4 + \frac{1}{L_s} \cdot v_s(t), \frac{-1}{C_{dc} \cdot R_{dc}} \cdot x_4 + \frac{1}{C_{dc}} \cdot m_r(t)^T \cdot (x_1 \ x_2 \ x_3)^T \right)$$

$$CI := (-22.073 \ 9.004 \ 13.069 \ 191.267)^T Z := \text{rkfixed}(CI, 0, t_f, n_f, D)$$

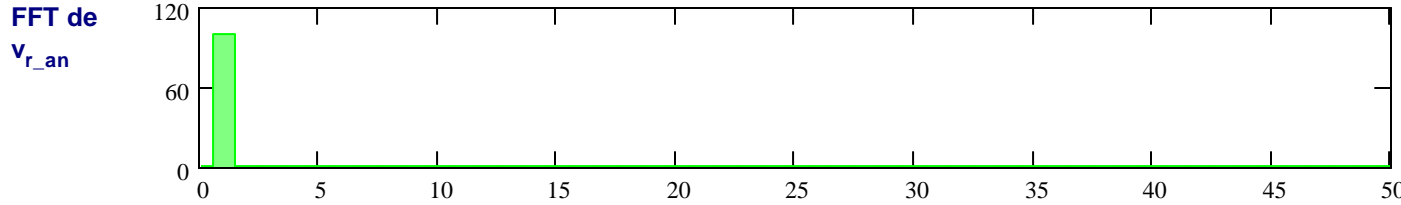
$$CI := \begin{pmatrix} Z_{n_f,2} & Z_{n_f,3} & Z_{n_f,4} & Z_{n_f,5} \end{pmatrix}^T Z := \text{rkfixed}(CI, 0, t_f, n_f, D)$$

$$v_{dc}(n) := Z_{n,5} \quad v_{r_an}(t) := \left(m_r(t) \cdot v_{dc} \left(t \cdot \frac{n_f}{t_f} \right) \right)_1 \quad v_{r_bn}(t) := \left(m_r(t) \cdot v_{dc} \left(t \cdot \frac{n_f}{t_f} \right) \right)_2 \quad v_{r_cn}(t) := \left(m_r(t) \cdot v_{dc} \left(t \cdot \frac{n_f}{t_f} \right) \right)_3$$

$$i_{r_a}(n) := Z_{n,2} \quad i_{r_b}(n) := Z_{n,3} \quad i_{r_c}(n) := Z_{n,4} \quad i_{dc}(n) := \left(m_r \left(n \cdot \frac{t_f}{n_f} \right) \right) \cdot (i_{r_a}(n) \ i_{r_b}(n) \ i_{r_c}(n))^T$$

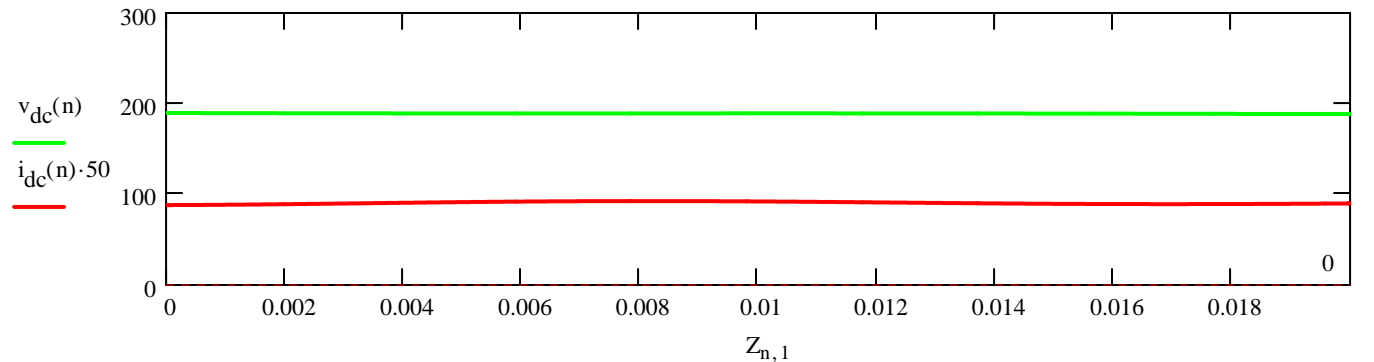


```
N := 1024      m := 1..N
x_m := v_r_an(m/N * t_f)  xf := FFT(x)
xv(m) := if(m = 1, 1, 2) * xf_m_per
|xv(2)| = 99.254
```

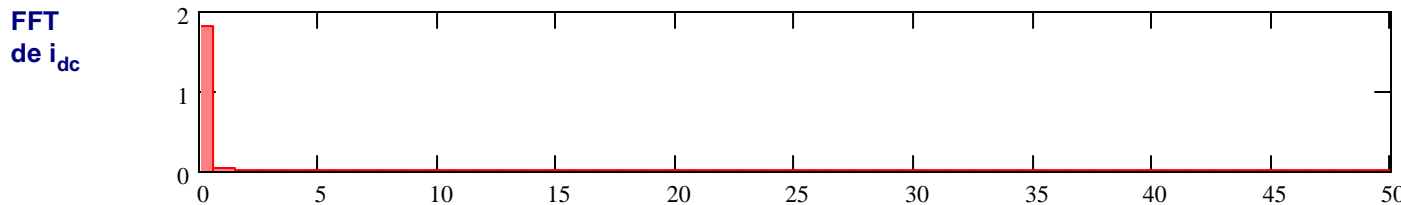


$$\frac{1}{2} \cdot M \cdot v_{dc}(1) = 99.554$$

La fundamental de voltaje de fase es igual a la moduladora sobre 2.



```
N := 1024      m := 1..N
x_m := i_dc(m/N * n_f)  xf := FFT(x)
xv(m) := if(m = 1, 1, 2) * xf_m_per
|xv(1)| = 1.808  I_dc := |xv(1)|
```



$$P_O := R_{dc} \cdot I_{dc}^2$$

$$P_O = 327.065$$

Modelo Promedio dq0 de Rectificador de Voltaje Trifásico

Problema Estudiar el modelo promedio en dq0 del rectificador de voltaje.

$$v_{rdq_n}(t) = m_{rdq}(t) \cdot v_{dc}(t)$$

$$i_{dc}(t) = m_{rdq}(t)^T \cdot i_{rdq}(t)$$

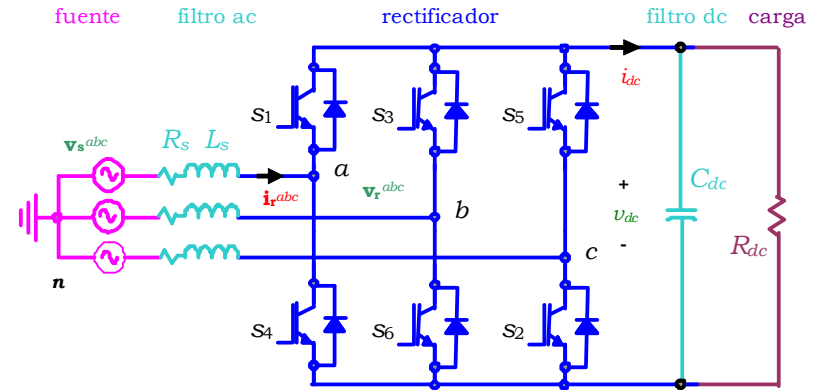
$$v_{sdq}(t) = R_s \cdot i_{rdq}(t) + L_s \cdot (di_{rdq}(t) + W \cdot i_{rdq}(t)) + m_{rdq}(t) \cdot v_{dc}(t)$$

$$m_{rdq}(t)^T \cdot i_{rdq}(t) = C_{dc} \cdot dv_{dc}(t) + \frac{v_{dc}(t)}{R_{dc}}$$

$$di_{rdq}(t) = -W \cdot i_{rdq}(t) + \frac{-R_s}{L_s} \cdot i_{rdq}(t) - \frac{1}{L_s} \cdot m_{rdq}(t) \cdot v_{dc}(t) + \frac{1}{L_s} \cdot v_{sdq}(t)$$

$$dv_{dc}(t) = \frac{-1}{C_{dc} \cdot R_{dc}} \cdot v_{dc}(t) + \frac{1}{C_{dc}} \cdot m_{rdq}(t)^T \cdot i_{rdq}(t)$$

$$v_{sdq}(t) := (\sqrt{3} \cdot 220 \ 0)^T$$



Parámetros

$$L_s := 30 \cdot 10^{-3}$$

$$R_s := 1$$

$$C_{dc} := 500 \cdot 10^{-6}$$

$$R_{dc} := 100$$

$$W := \begin{pmatrix} 0 & -\omega_s \\ \omega_s & 0 \end{pmatrix}$$

$$m_{rdq}(t) := \sqrt{\frac{2}{3}} \cdot \begin{pmatrix} \sin(\omega_s \cdot t) & \sin(\omega_s \cdot t - 2 \cdot \frac{\pi}{3}) & \sin(\omega_s \cdot t - 4 \cdot \frac{\pi}{3}) \\ \cos(\omega_s \cdot t) & \cos(\omega_s \cdot t - 2 \cdot \frac{\pi}{3}) & \cos(\omega_s \cdot t - 4 \cdot \frac{\pi}{3}) \end{pmatrix} \cdot m_r(t)$$

Simulación $t_f := 0.02$ $n_f := 2048$ $n := 1 .. n_f$ $t := 0, \frac{t_f}{n_f} .. t_f$

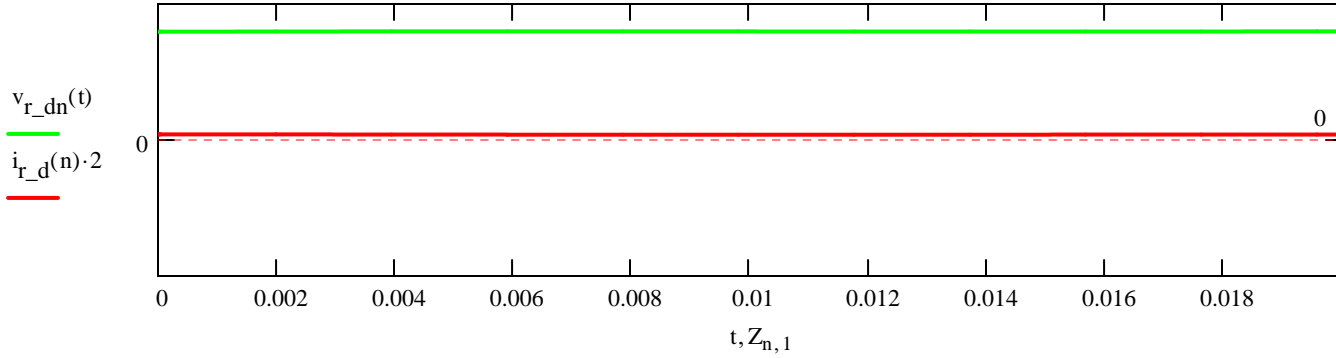
$$D(t, x) := \text{stack} \left(-W \cdot (x_1 \ x_2)^T + \frac{-R_s}{L_s} \cdot (x_1 \ x_2)^T - \frac{1}{L_s} \cdot m_{rdq}(t) \cdot x_3 + \frac{1}{L_s} \cdot v_{sdq}(t), \frac{-1}{C_{dc} \cdot R_{dc}} \cdot x_3 + \frac{1}{C_{dc}} \cdot m_{rdq}(t)^T \cdot (x_1 \ x_2)^T \right)$$

$$CI := (2.948 \ -27.293 \ 184.503)^T \quad Z := \text{rkfixed}(CI, 0, t_f, n_f, D) \quad CI := \begin{pmatrix} Z_{n_f, 2} & Z_{n_f, 3} & Z_{n_f, 4} \end{pmatrix}^T \quad Z := \text{rkfixed}(CI, 0, t_f, n_f, D)$$

$$v_{dc}(n) := Z_{n,4} \quad v_{r_dn}(t) := \left(m_{rdq}(t) \cdot v_{dc} \left(t \cdot \frac{n_f}{t_f} \right) \right)_1 \quad v_{r_qn}(t) := \left(m_{rdq}(t) \cdot v_{dc} \left(t \cdot \frac{n_f}{t_f} \right) \right)_2$$

$$i_{r_d}(n) := Z_{n,2} \quad i_{r_q}(n) := Z_{n,3}$$

$$i_{dc}(n) := \left(m_{rdq} \left(n \cdot \frac{t_f}{n_f} \right) \right)^T \cdot \left(i_{r_d}(n) \quad i_{r_q}(n) \right)^T$$



$$N := 1024 \quad m := 1 \dots N$$

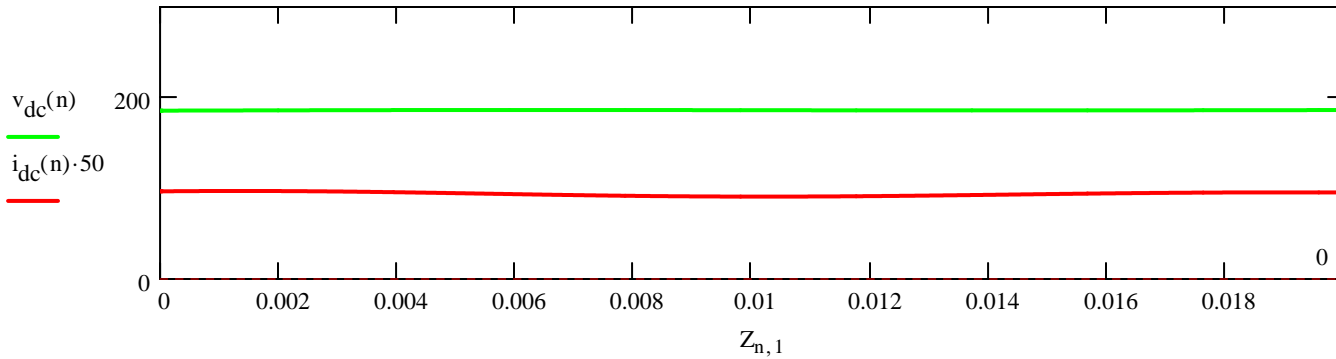
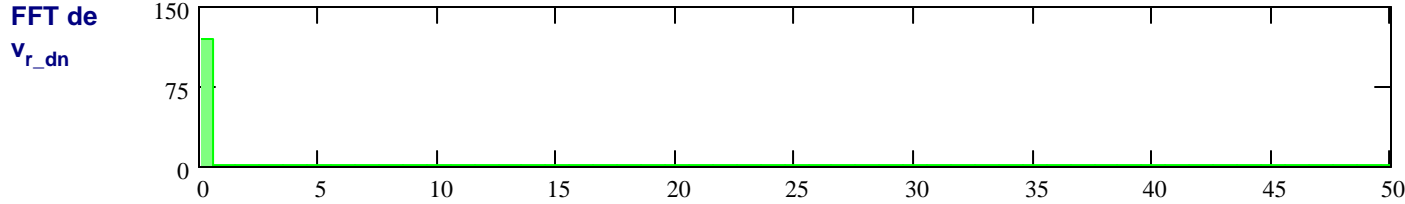
$$x_m := v_{r_dn} \left(\frac{m}{N} \cdot t_f \right) \quad xf := \text{FFT}(x)$$

$$xv(m) := \text{if}(m = 1, 1, 2) \cdot xf_{m\text{-per}}$$

$$\sqrt{\frac{2}{3}} \cdot \sqrt{v_{r_dn}(0.01)^2 + v_{r_qn}(0.01)^2} = 97.697$$

$$\sqrt{\frac{2}{3}} \cdot |m_{rdq}(0.01)| \cdot v_{dc}(1) = 97.44$$

$$\frac{1}{2} \cdot M \cdot v_{dc}(1) = 97.44$$



$$N := 1024 \quad m := 1 \dots N$$

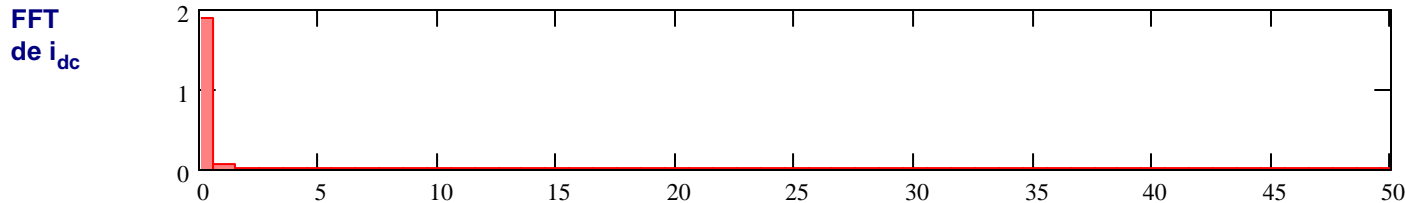
$$x_m := i_{dc} \left(\frac{m}{N} \cdot n_f \right) \quad xf := \text{FFT}(x)$$

$$xv(m) := \text{if}(m = 1, 1, 2) \cdot xf_{m\text{-per}}$$

$$|xv(1)| = 1.876 \quad I_{dc} := |xv(1)|$$

$$P_o := R_{dc} \cdot I_{dc}^2$$

$$P_o = 352.03$$



Punto de operación del Rectificador de Voltaje Trifásico en dq0

Problema Encontrar un punto de operación

$$\phi_0 := -30 \cdot \frac{\pi}{180}$$

$$P_{dc_0} := 5000$$

$$\begin{pmatrix} V_{sd} \\ V_{sq} \end{pmatrix} := \begin{pmatrix} \sqrt{3} \cdot 220 \\ 0 \end{pmatrix}$$

c.i. para Given/Find que deben ser igual en número al número de incógnitas

$$\begin{pmatrix} I_{rd} \\ I_{rq} \end{pmatrix} := \begin{pmatrix} 10 \\ 0 \end{pmatrix}$$

$$\begin{pmatrix} M_{rd} \\ M_{rq} \end{pmatrix} := \begin{pmatrix} 0.5 \\ 0 \end{pmatrix}$$

$$V_{dc} := 500$$

Given

$$\begin{pmatrix} 0 \\ 0 \end{pmatrix} = -W \cdot \begin{pmatrix} I_{rd} \\ I_{rq} \end{pmatrix} + \frac{-R_s}{L_s} \cdot \begin{pmatrix} I_{rd} \\ I_{rq} \end{pmatrix} - \frac{1}{L_s} \cdot \begin{pmatrix} M_{rd} \\ M_{rq} \end{pmatrix} \cdot V_{dc} + \frac{1}{L_s} \cdot \begin{pmatrix} V_{sd} \\ V_{sq} \end{pmatrix}$$

$$0 = \frac{-1}{C_{dc} \cdot R_{dc}} \cdot V_{dc} + \frac{1}{C_{dc}} \cdot \begin{pmatrix} M_{rd} \\ M_{rq} \end{pmatrix}^T \cdot \begin{pmatrix} I_{rd} \\ I_{rq} \end{pmatrix}$$

$$\phi_0 = \text{atan} \left(\frac{I_{rq}}{I_{rd}} \right)$$

$$P_{dc_0} = \frac{V_{dc}^2}{R_{dc}}$$

$$\begin{pmatrix} I_{rd} & I_{rq} & V_{dc} & M_{rd} & M_{rq} \end{pmatrix} := \text{Find}(I_{rd}, I_{rq}, V_{dc}, M_{rd}, M_{rq})^T$$

$$\begin{pmatrix} I_{rd} & I_{rq} & V_{dc} & M_{rd} & M_{rq} \end{pmatrix} = (13.787 \quad -7.96 \quad 707.107 \quad 0.413 \quad -0.173)$$

$$m_{rdq}(t) := \begin{pmatrix} M_{rd} & M_{rq} \end{pmatrix}^T$$

$$v_{sdq}(t) := \begin{pmatrix} V_{sd} & 0 \end{pmatrix}^T$$

$$T_{abc_dq0}(t) := \sqrt{\frac{2}{3}} \cdot \begin{pmatrix} \sin(\omega_s \cdot t) & \sin(\omega_s \cdot t - 2 \cdot \frac{\pi}{3}) & \sin(\omega_s \cdot t - 4 \cdot \frac{\pi}{3}) \\ \cos(\omega_s \cdot t) & \cos(\omega_s \cdot t - 2 \cdot \frac{\pi}{3}) & \cos(\omega_s \cdot t - 4 \cdot \frac{\pi}{3}) \\ \frac{1}{\sqrt{2}} & \frac{1}{\sqrt{2}} & \frac{1}{\sqrt{2}} \end{pmatrix}$$

Simulación $t_f := 0.02$ $n_f := 2048$ $n := 1..n_f$ $t := 0, \frac{t_f}{n_f} .. t_f$

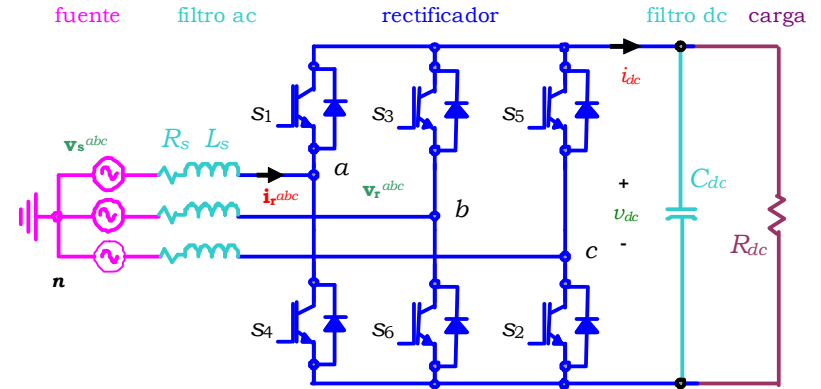
$$D(t, x) := \text{stack} \left(-W \cdot \begin{pmatrix} x_1 & x_2 \end{pmatrix}^T + \frac{-R_s}{L_s} \cdot \begin{pmatrix} x_1 & x_2 \end{pmatrix}^T - \frac{1}{L_s} \cdot m_{rdq}(t) \cdot x_3 + \frac{1}{L_s} \cdot v_{sdq}(t), \frac{-1}{C_{dc} \cdot R_{dc}} \cdot x_3 + \frac{1}{C_{dc}} \cdot \left((m_{rdq}(t))^T \cdot \begin{pmatrix} x_1 & x_2 \end{pmatrix} \right)^T \right)$$

$$CI := \begin{pmatrix} I_{rd} & I_{rq} & V_{dc} \end{pmatrix}^T$$

$$Z := \text{rkfixed}(CI, 0, t_f, n_f, D)$$

$$CI := \begin{pmatrix} Z_{n_f, 2} & Z_{n_f, 3} & Z_{n_f, 4} \end{pmatrix}^T$$

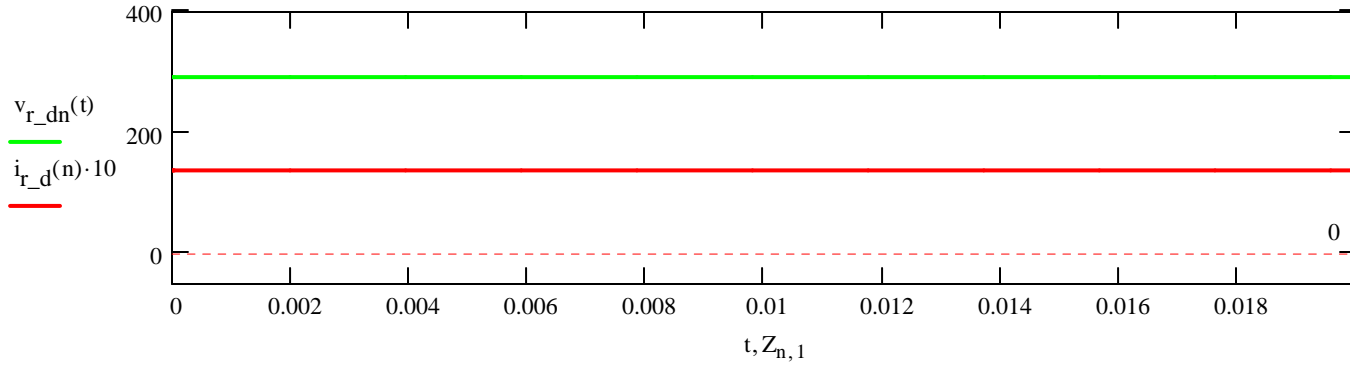
$$Z := \text{rkfixed}(CI, 0, t_f, n_f, D)$$



$$v_{dc}(n) := Z_{n,4} \quad v_{r_dn}(t) := \left(m_{rdq}(t) \cdot v_{dc} \left(t \cdot \frac{n_f}{t_f} \right) \right)_1 \quad v_{r_qn}(t) := \left(m_{rdq}(t) \cdot v_{dc} \left(t \cdot \frac{n_f}{t_f} \right) \right)_2$$

$$i_{r_d}(n) := Z_{n,2} \quad i_{r_q}(n) := Z_{n,3}$$

$$i_{dc}(n) := \left(m_{rdq} \left(n \cdot \frac{t_f}{n_f} \right) \right)^T \cdot (i_{r_d}(n) \quad i_{r_q}(n))^T$$



$$N := 1024 \quad m := 1..N$$

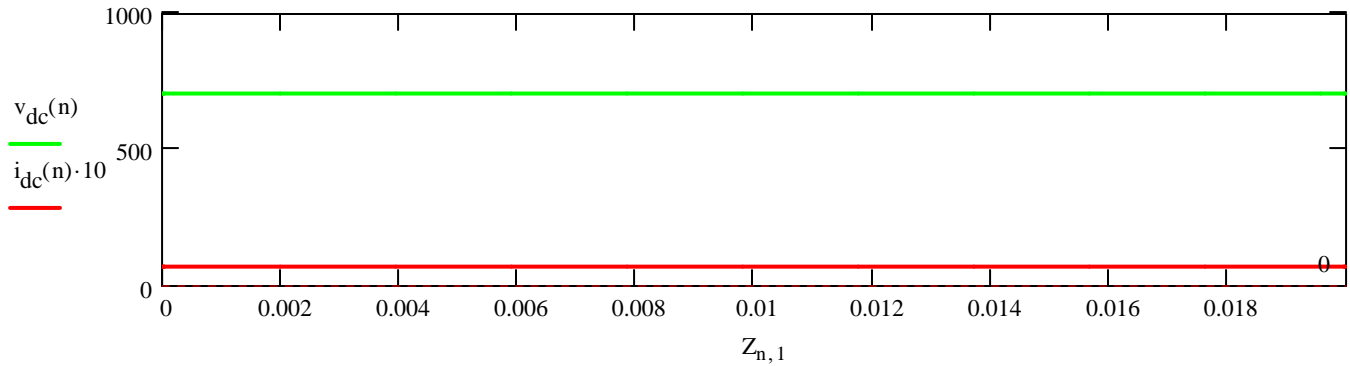
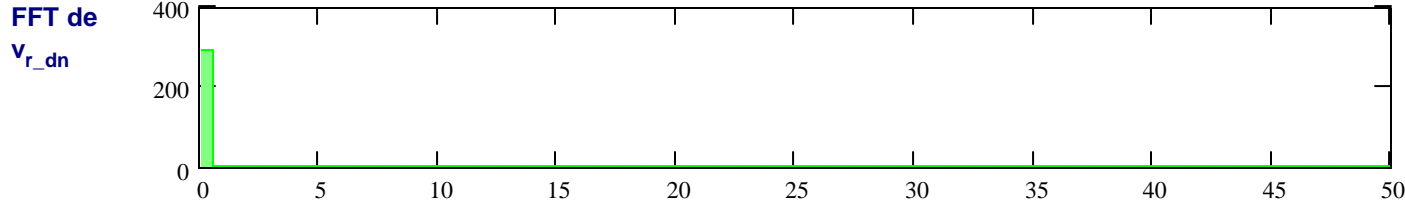
$$x_m := v_{r_dn} \left(\frac{m}{N} \cdot t_f \right) \quad xf := \text{FFT}(x)$$

$$xv(m) := \text{if}(m = 1, 1, 2) \cdot xf_{m\text{-per}}$$

$$\sqrt{\frac{2}{3}} \cdot \sqrt{v_{r_dn}(0.01)^2 + v_{r_qn}(0.01)^2} = 258.568$$

$$\sqrt{\frac{2}{3}} \cdot |m_{rdq}(0.01)| \cdot v_{dc}(1) = 258.568$$

$$\text{atan} \left(\frac{i_{r_q}(1)}{i_{r_d}(1)} \right) \cdot \frac{180}{\pi} = -30$$



$$N := 1024 \quad m := 1..N$$

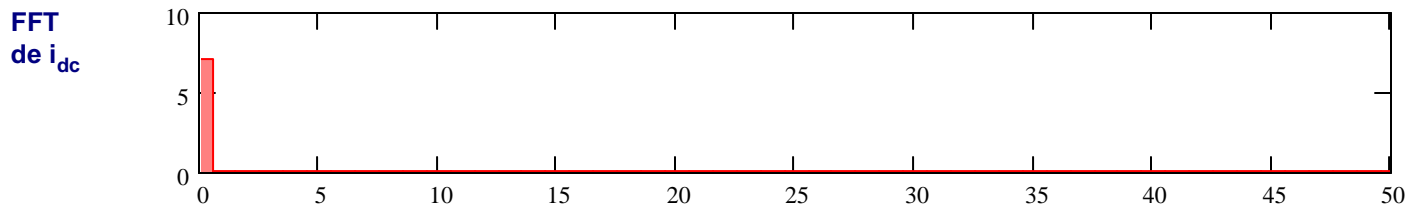
$$x_m := i_{dc} \left(\frac{m}{N} \cdot n_f \right) \quad xf := \text{FFT}(x)$$

$$xv(m) := \text{if}(m = 1, 1, 2) \cdot xf_{m\text{-per}}$$

$$|xv(1)| = 7.071 \quad I_{dc} := |xv(1)|$$

$$P_o := R_{dc} \cdot I_{dc}^2$$

$$P_o = 5 \times 10^3$$



Punto de operación del Rectificador de Voltaje Trifásico en abc

Problema Simular el punto de operación.

$$di_r(t) = \frac{-R_s}{L_s} \cdot i_r(t) - \frac{1}{L_s} \cdot T_{\text{In}} \cdot s_r(t) \cdot v_{\text{dc}}(t) + \frac{1}{L_s} \cdot v_s(t)$$

$$dv_{\text{dc}}(t) = \frac{-1}{C_{\text{dc}} \cdot R_{\text{dc}}} \cdot v_{\text{dc}}(t) + \frac{1}{C_{\text{dc}}} \cdot s_r(t)^T \cdot T_{\text{In}} \cdot i_r(t)$$

$$m_r(t) := T_{\text{abc_dq0}}(t)^T \cdot \begin{pmatrix} M_{\text{rd}} \\ M_{\text{rq}} \\ 0 \end{pmatrix}$$

$$m_a(t) := 2 \cdot m_r(t)_1$$

$$m_b(t) := 2 \cdot m_r(t)_2$$

$$m_c(t) := 2 \cdot m_r(t)_3$$

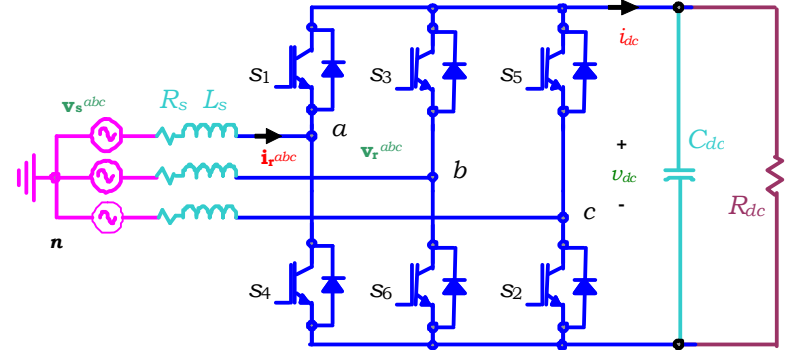
$$M := \sqrt{\frac{2}{3} \cdot m_a(0)^2 + m_b(0)^2 + m_c(0)^2}$$

$$f_M := \text{atan}\left(\frac{M_{\text{rq}}}{M_{\text{rd}}}\right)$$

$$M = 0.731$$

$$f_M \cdot \frac{180}{\pi} = -22.655$$

fuelle filtro ac rectificador filtro dc carga



$$\text{tri}(t) := \frac{2}{\pi} \cdot \text{asin}\left(\sin\left(f_{\text{n_tr}} \cdot \omega_s \cdot t + f_M \cdot f_{\text{n_tr}} - \pi\right)\right)$$

$$\text{sup}(t) := \text{if}(m_a(t) > m_b(t), \text{if}(m_a(t) > m_c(t), m_a(t), m_c(t)), \text{if}(m_b(t) > m_c(t), m_b(t), m_c(t)))$$

$$\text{inf}(t) := \text{if}(m_a(t) < m_b(t), \text{if}(m_a(t) < m_c(t), m_a(t), m_c(t)), \text{if}(m_b(t) < m_c(t), m_b(t), m_c(t))) \quad \text{seq}_0(t) := (\text{sup}(t) + \text{inf}(t)) \cdot \frac{1}{3}$$

$$m_{a0}(t) := m_a(t) - \text{seq}_0(t)$$

$$m_{b0}(t) := m_b(t) - \text{seq}_0(t)$$

$$m_{c0}(t) := m_c(t) - \text{seq}_0(t)$$

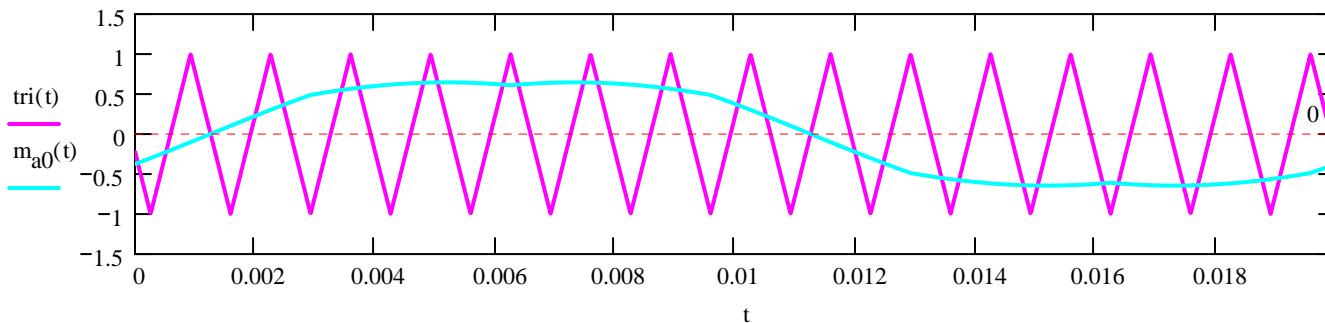
$$s_1(t) := \text{if}(m_{a0}(t) > \text{tri}(t), 1, 0)$$

$$s_3(t) := \text{if}(m_{b0}(t) > \text{tri}(t), 1, 0)$$

$$s_5(t) := \text{if}(m_{c0}(t) > \text{tri}(t), 1, 0)$$

$$s_r(t) := \begin{pmatrix} s_1(t) \\ s_3(t) \\ s_5(t) \end{pmatrix}$$

$$v_s(t) := T_{\text{abc_dq0}}(t)^T \cdot \begin{pmatrix} V_{\text{sd}} \\ V_{\text{sq}} \\ 0 \end{pmatrix}$$



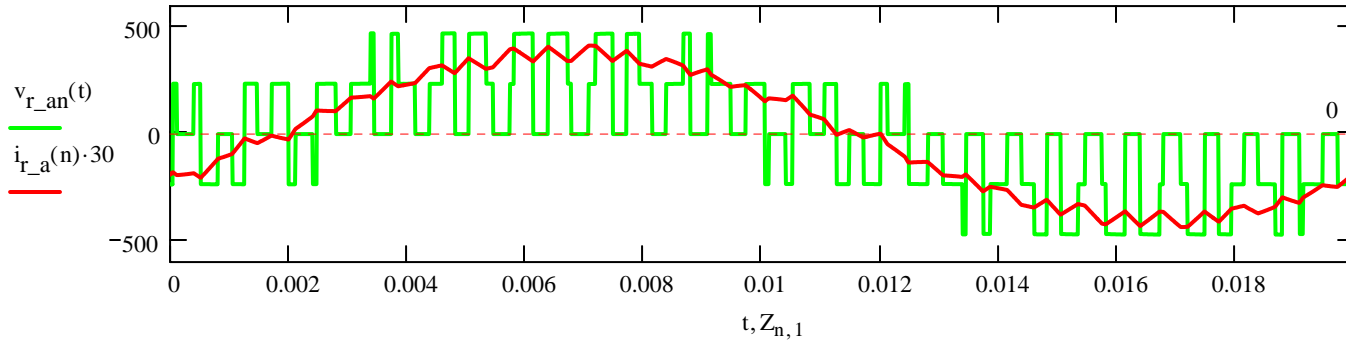
Simulación $t_f := 0.02$ $n_f := 2048$ $n := 1 .. n_f$ $t := 0, \frac{t_f}{n_f} .. t_f$

$$D(t, x) := \text{stack}\left(\frac{-R_s}{L_s} \cdot (x_1 \ x_2 \ x_3)^T - \frac{1}{L_s} \cdot T_{\text{In}} \cdot s_r(t) \cdot x_4 + \frac{1}{L_s} \cdot v_s(t), \frac{-1}{C_{\text{dc}} \cdot R_{\text{dc}}} \cdot x_4 + \frac{1}{C_{\text{dc}}} \cdot (s_r(t))^T \cdot T_{\text{In}} \cdot (x_1 \ x_2 \ x_3)^T\right)$$

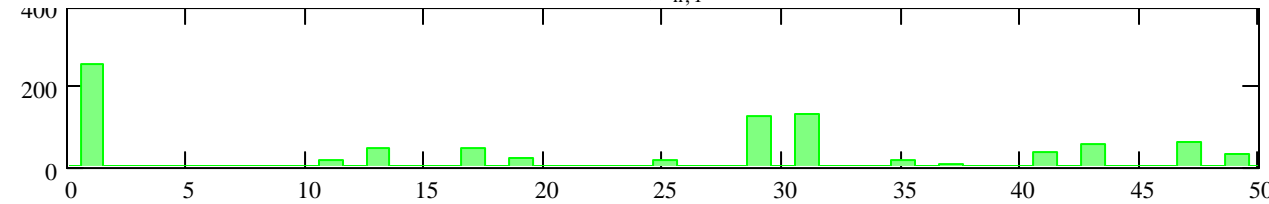
$$CI := \text{stack}\left(T_{abc_dq0}(0)^T \cdot (I_{rd} \ I_{rq} \ 0)^T, V_{dc}\right) \quad Z := \text{rkfixed}(CI, 0, t_f, n_f, D) \quad CI := \begin{pmatrix} Z_{n_f,2} & Z_{n_f,3} & Z_{n_f,4} & Z_{n_f,5} \end{pmatrix}^T \quad Z := \text{rkfixed}(CI, 0, t_f, n_f, D)$$

$$v_{dc}(n) := Z_{n,5} \quad v_{r_an}(t) := \left(T_{ln} \cdot s_r(t) \cdot v_{dc} \left(t \cdot \frac{n_f}{t_f} \right) \right)_1 \quad v_{r_bn}(t) := \left(T_{ln} \cdot s_r(t) \cdot v_{dc} \left(t \cdot \frac{n_f}{t_f} \right) \right)_2 \quad v_{r_cn}(t) := \left(T_{ln} \cdot s_r(t) \cdot v_{dc} \left(t \cdot \frac{n_f}{t_f} \right) \right)_3$$

$$i_{r_a}(n) := Z_{n,2} \quad i_{r_b}(n) := Z_{n,3} \quad i_{r_c}(n) := Z_{n,4} \quad i_{dc}(n) := \left(s_r \left(n \cdot \frac{t_f}{n_f} \right) \right)^T \cdot (T_{ln})^T \cdot (i_{r_a}(n) \ i_{r_b}(n) \ i_{r_c}(n))^T$$

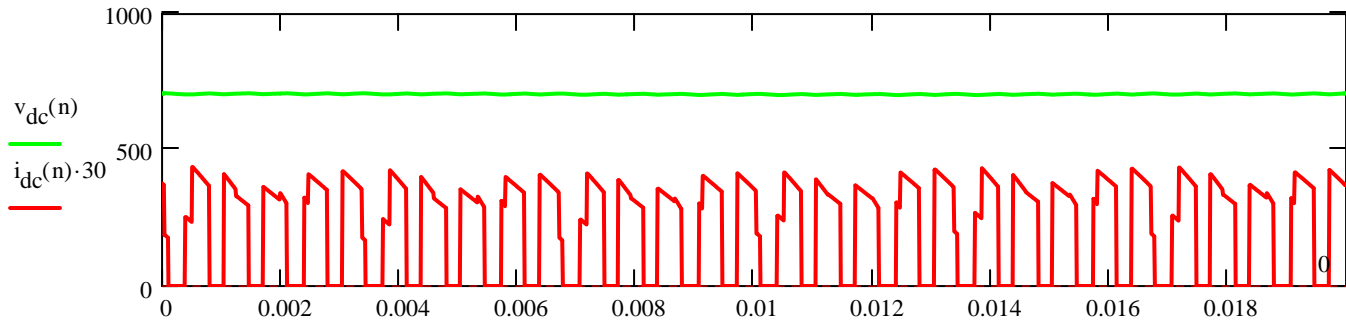


FFT de v_{r_an}

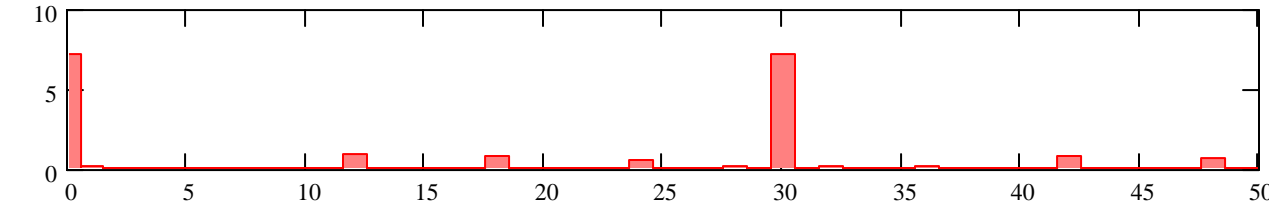


$N := 1024$ $m := 1 \dots N$
 $x_m := v_{r_an} \left(\frac{m}{N} \cdot t_f \right)$ $xf := \text{FFT}(x)$
 $xv(m) := \text{if}(m = 1, 1, 2) \cdot xf_{m\text{-per}}$
 $|xv(2)| = 257.318$
 $\frac{1}{2} \cdot M \cdot v_{dc}(1) = 258.83$

La fundamental de voltaje de fase es igual a la moduladora sobre 2.



FFT de i_{dc}



$N := 1024$ $m := 1 \dots N$
 $x_m := i_{dc} \left(\frac{m}{N} \cdot n_f \right)$ $xf := \text{FFT}(x)$
 $xv(m) := \text{if}(m = 1, 1, 2) \cdot xf_{m\text{-per}}$
 $|xv(1)| = 7.126$ $I_{dc} := |xv(1)|$
 $P_o := R_{dc} \cdot I_{dc}^2$
 $P_o = 5.078 \times 10^3$

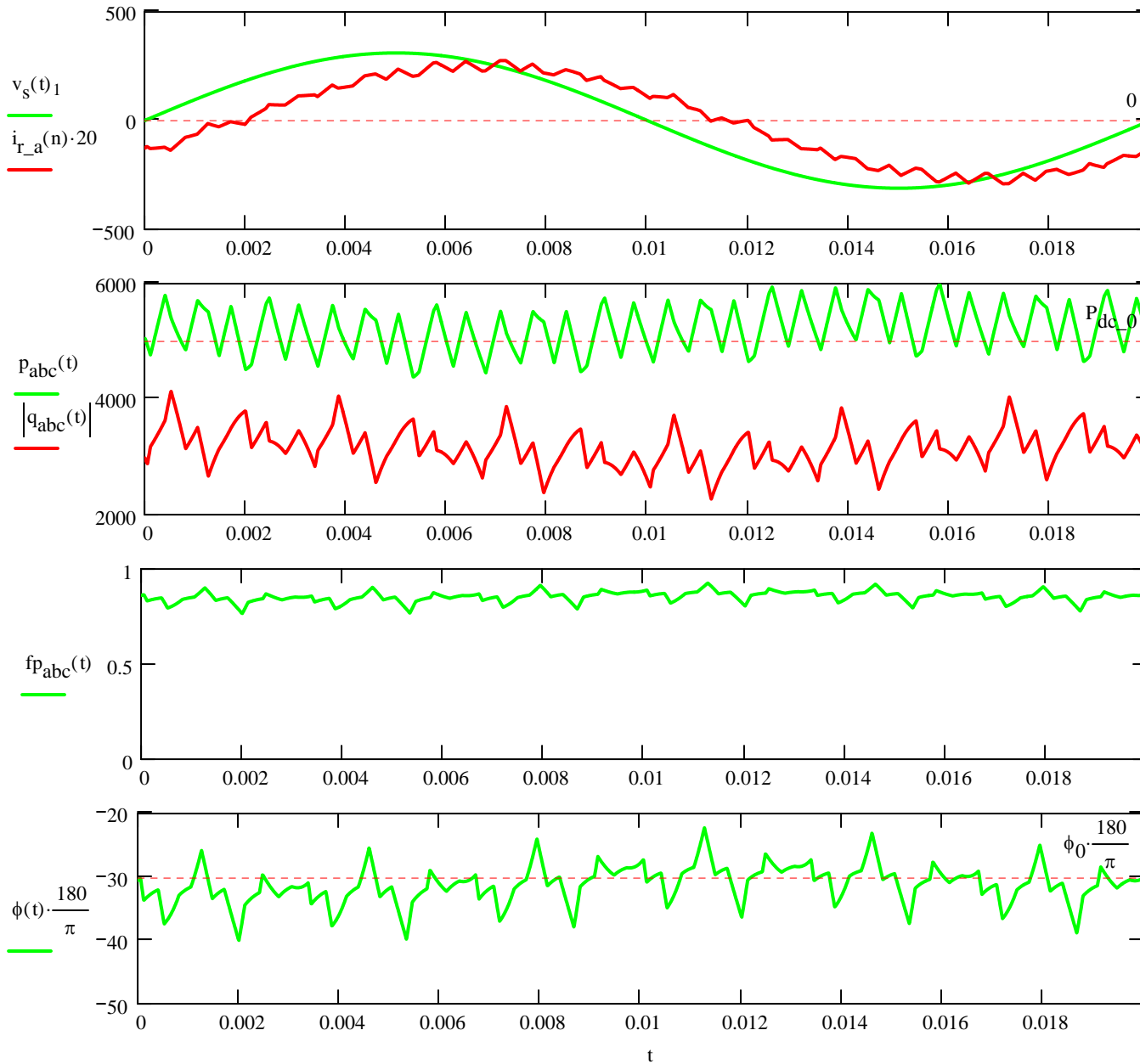
$$v_{abc}(t) := v_s(t) \quad i_{abc}(t) := \left(i_{r_a} \left(t \cdot \frac{n_f}{t_f} \right) \quad i_{r_b} \left(t \cdot \frac{n_f}{t_f} \right) \quad i_{r_c} \left(t \cdot \frac{n_f}{t_f} \right) \right)^T \quad p_{abc}(t) := v_{abc}(t)^T \cdot i_{abc}(t)$$

$$q_{abc}(t) := v_{abc}(t) \times i_{abc}(t)$$

$$s_{abc}(t) := \sqrt{(|v_{abc}(t)|)^2 \cdot (|i_{abc}(t)|)^2}$$

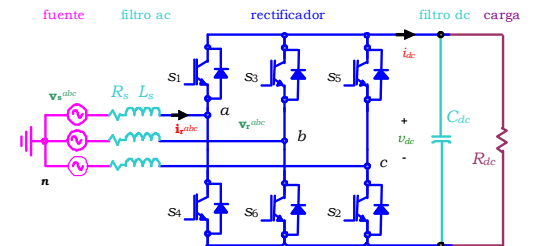
$$fp_{abc}(t) := \frac{p_{abc}(t)}{s_{abc}(t)}$$

$$\phi(t) := \text{atan} \left[\frac{(T_{abc_dq0}(t) \cdot i_{abc}(t))_2}{(T_{abc_dq0}(t) \cdot i_{abc}(t))_1} \right]$$



El sistema todavía no está en S.S.

¿ Qué rangos puede alcanzar el sistema ?... **La Región de Operación** entrega esta respuesta.



Región de Operación del RFV Trifásico en dq0

Problema Estudiar el modelo promedio en dq0 del rectificador de voltaje. $t := 0$

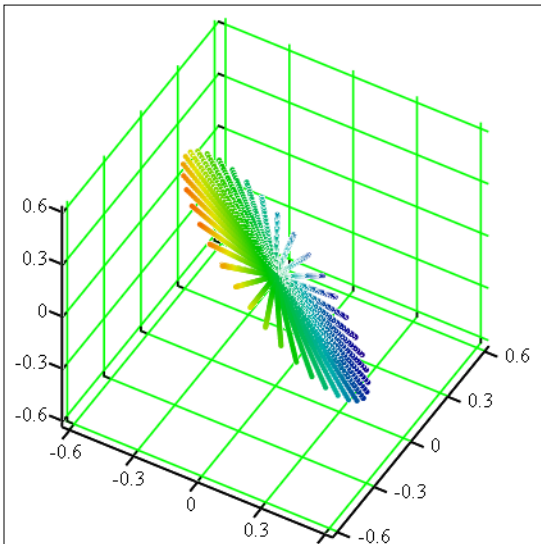
$$m_{r_abc}(M, f_M) := \frac{1}{2} \cdot \begin{pmatrix} M \cdot \sin\left(\omega_s \cdot t + f_M - \frac{0 \cdot \pi}{3}\right) \\ M \cdot \sin\left(\omega_s \cdot t + f_M - \frac{2 \cdot \pi}{3}\right) \\ M \cdot \sin\left(\omega_s \cdot t + f_M - \frac{4 \cdot \pi}{3}\right) \end{pmatrix}$$

$$X_a(M, f_M) := m_{r_abc}(M, f_M)_1$$

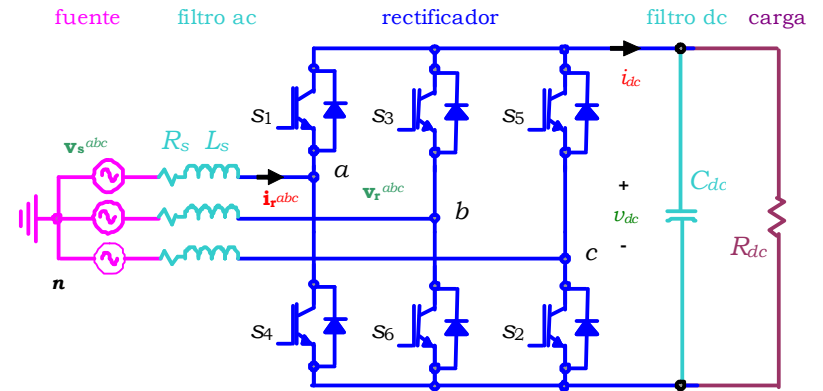
$$Y_b(M, f_M) := m_{r_abc}(M, f_M)_2$$

$$Z_c(M, f_M) := m_{r_abc}(M, f_M)_3$$

Las señales en abc en función de M y f_M .



(X_a, Y_b, Z_c)



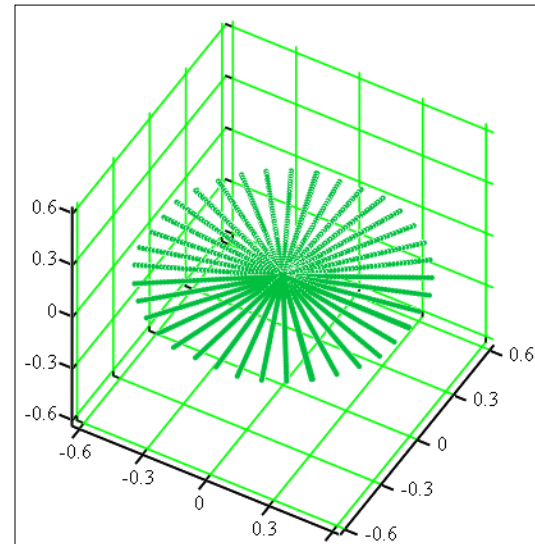
$$m_{r_dq0}(M, f_M) := T_{abc_dq0}(t) \cdot m_{r_abc}(M, f_M)$$

$$X_d(M, f_M) := m_{r_dq0}(M, f_M)_1$$

$$Y_q(M, f_M) := m_{r_dq0}(M, f_M)_2$$

$$Z_0(M, f_M) := m_{r_dq0}(M, f_M)_3$$

Las señales en dq0 en función de M y f_M .



(X_d, Y_q, Z_0)

c.i. para Given/Find que deben ser igual en número al número de incógnitas

$$\begin{pmatrix} I_{rd} \\ I_{rq} \end{pmatrix} := \begin{pmatrix} 10 \\ 0 \end{pmatrix}$$

$$\begin{pmatrix} M_{rd} \\ M_{rq} \end{pmatrix} := \begin{pmatrix} 0.5 \\ 0 \end{pmatrix}$$

$$V_{dc} := 500$$

$$\begin{pmatrix} V_{sd} \\ V_{sq} \end{pmatrix} := \begin{pmatrix} \sqrt{3} \cdot 220 \\ 0 \end{pmatrix}$$

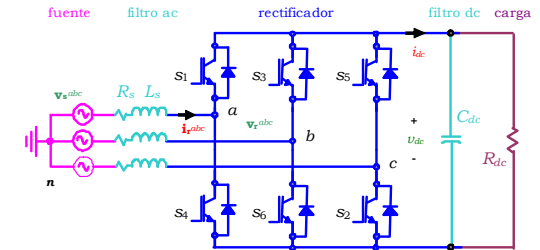
$$\text{Max} := \frac{1}{2} \cdot \sqrt{\frac{3}{2}}$$

Given

$$\begin{pmatrix} 0 \\ 0 \end{pmatrix} = -W \cdot \begin{pmatrix} I_{rd} \\ I_{rq} \end{pmatrix} + \frac{-R_s}{L_s} \cdot \begin{pmatrix} I_{rd} \\ I_{rq} \end{pmatrix} - \frac{1}{L_s} \cdot \begin{pmatrix} M_{rd} \\ M_{rq} \end{pmatrix} \cdot V_{dc} + \frac{1}{L_s} \cdot \begin{pmatrix} V_{sd} \\ V_{sq} \end{pmatrix}$$

$$0 = \frac{-1}{C_{dc} \cdot R_{dc}} \cdot V_{dc} + \frac{1}{C_{dc}} \cdot \begin{pmatrix} M_{rd} \\ M_{rq} \end{pmatrix}^T \cdot \begin{pmatrix} I_{rd} \\ I_{rq} \end{pmatrix}$$

$$\text{Sol}(M_{rd}, M_{rq}) := \text{Find}(I_{rd}, I_{rq}, V_{dc})$$



Se graficará para M_{rd} y M_{rq} en el rango -Max a Max.

$$me := 40 \quad mi_1 := -\text{Max} \quad ma_1 := \text{Max} \quad mi_2 := -\text{Max} \quad ma_2 := \text{Max}$$

A graficar I_{rd} , I_{rq} y V_{dc}

$$I_{rd}(x_d, x_q) := \text{Sol}(x_d, x_q)_1$$

$$I_{rq}(x_d, x_q) := \text{Sol}(x_d, x_q)_2$$

$$V_{dc}(x_d, x_q) := \text{Sol}(x_d, x_q)_3$$

$$S_{I_{rd}} := \text{CreateMesh}(I_{rd}, mi_2, ma_2, mi_1, ma_1, me)$$

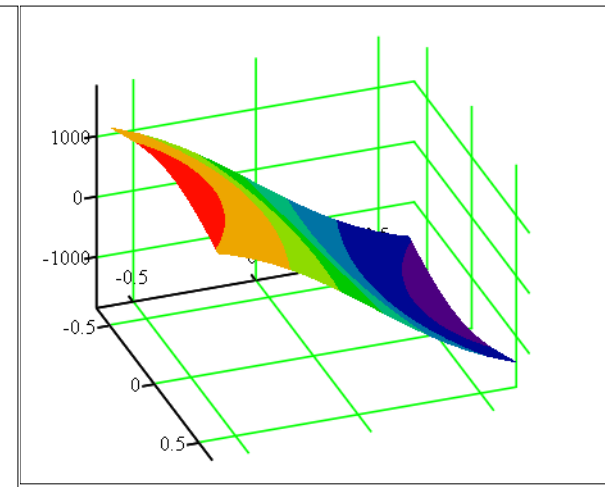
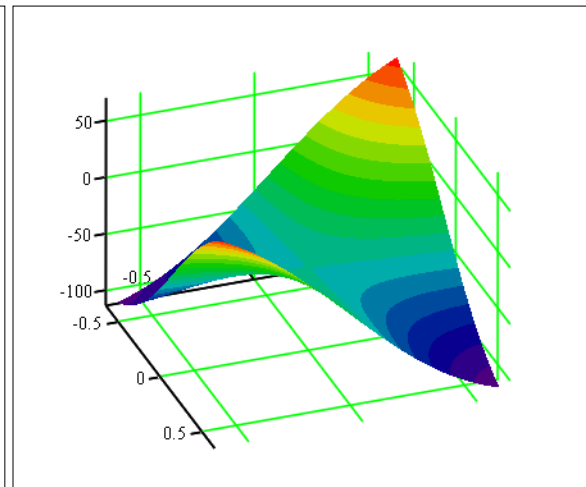
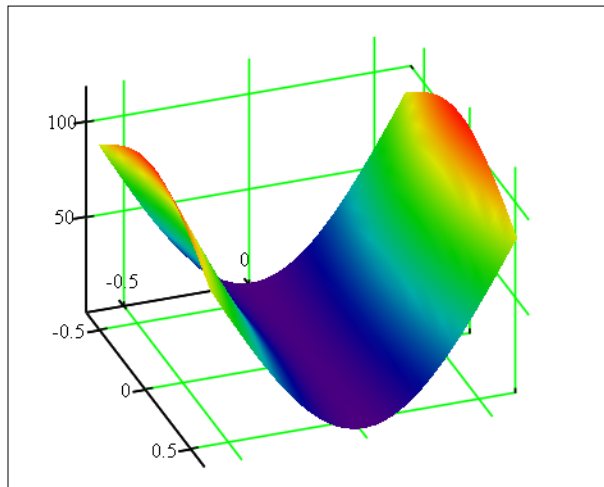
$$S_{I_{rq}} := \text{CreateMesh}(I_{rq}, mi_2, ma_2, mi_1, ma_1, me)$$

$$S_{V_{dc}} := \text{CreateMesh}(V_{dc}, mi_2, ma_2, mi_1, ma_1, me)$$

Corriente I_{rd}

Corriente I_{rq}

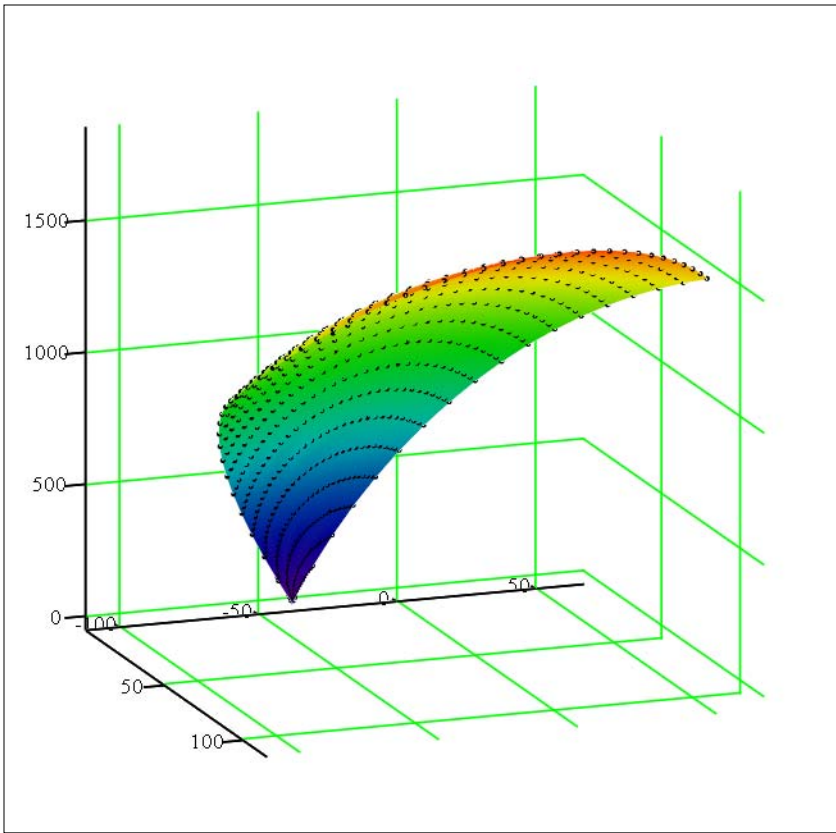
Voltaje V_{dc}



$S_{I_{rd}}$

$S_{I_{rq}}$

$S_{V_{dc}}$

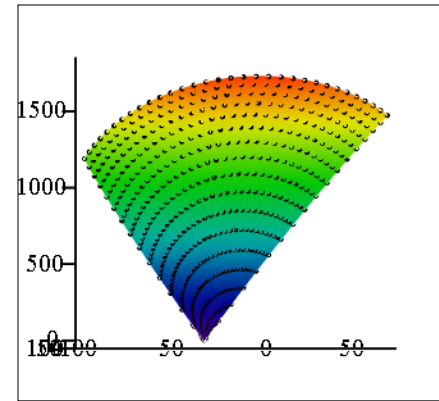


(I_{rd}, I_{rq}, V_{dc})

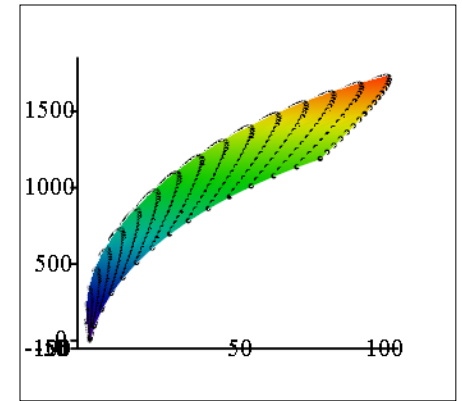
La tensión V_{dc} negativa no es opción, por los diodos en antiparalelo de la topología.

Hay dos entradas M_{rd} y M_{rq} y hay tres variables de estado. Las potenciales salidas podrían ser I_{rd} e I_{rq} , I_{rd} y V_{dc} , V_{dc} e I_{rq} .

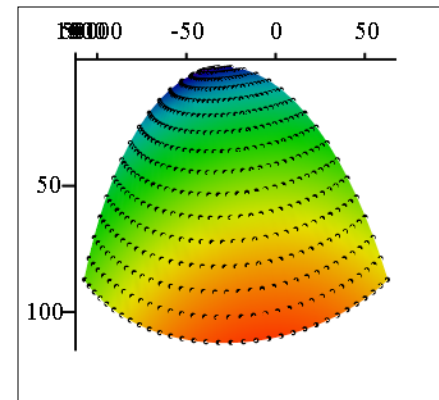
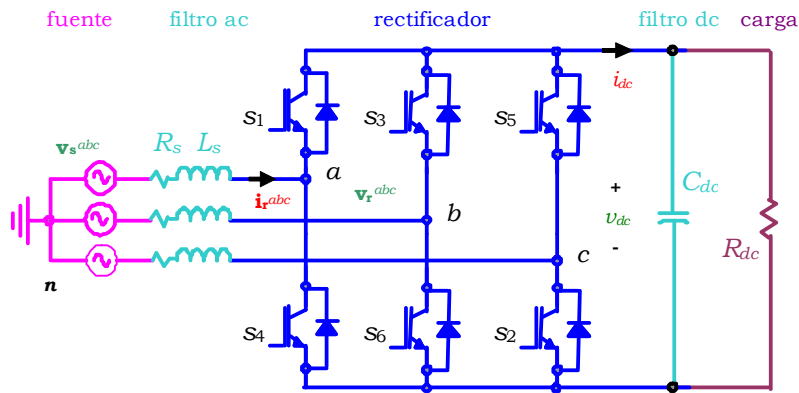
Es posible controlar I_{rd} e I_{rq} , V_{dc} e I_{rq} , pero **NO** se puede controlar I_{rd} y V_{dc} por el rango mínimo.



(I_{rd}, I_{rq}, V_{dc})



(I_{rd}, I_{rq}, V_{dc})



(I_{rd}, I_{rq}, V_{dc})

Inversor de Corriente Trifásico

Problema Estudiar el inversor de corriente con Modulación SPWM.

La moduladora es, $M := 1$ $\omega_s := 2 \cdot \pi \cdot 50$ $f_M := \frac{\pi}{6}$

La triangular es, $f_{n_tr} := 15$ per := 1

$$tri(t) := \frac{2}{\pi} \cdot asin(\sin(f_{n_tr} \cdot \omega_s \cdot t + f_M \cdot f_{n_tr} + \pi))$$

$$m_a(t, M) := M \cdot \sin\left(\omega_s \cdot t + f_M - \frac{0 \cdot \pi}{3}\right)$$

$$m_b(t, M) := M \cdot \sin\left(\omega_s \cdot t + f_M - \frac{2 \cdot \pi}{3}\right)$$

$$m_c(t, M) := M \cdot \sin\left(\omega_s \cdot t + f_M - \frac{4 \cdot \pi}{3}\right)$$

Auxiliar 1 $s_x(t) := if(m_a(t, M) > tri(t), 1, 0)$

Auxiliar 2 $s_y(t) := if(m_b(t, M) > tri(t), 1, 0)$

Auxiliar 3 $s_z(t) := if(m_c(t, M) > tri(t), 1, 0)$

$$s_{xn}(t) := if(s_x(t) = 1, 0, 1)$$

$$s_{yn}(t) := if(s_y(t) = 1, 0, 1)$$

$$s_{zn}(t) := if(s_z(t) = 1, 0, 1)$$

1ra pierna $s_1(t) := s_x(t) \cdot s_{zn}(t)$

2da pierna $s_3(t) := s_y(t) \cdot s_{xn}(t)$

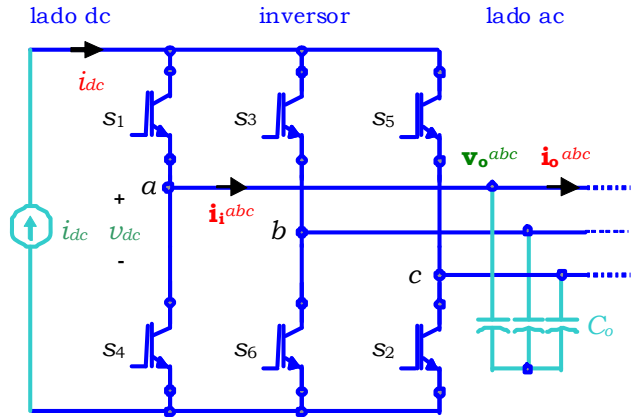
3ra pierna $s_5(t) := s_z(t) \cdot s_{yn}(t)$

$$s_4(t) := s_z(t) \cdot s_{xn}(t)$$

$$s_6(t) := s_x(t) \cdot s_{yn}(t)$$

$$s_2(t) := s_y(t) \cdot s_{zn}(t)$$

$$n_f := f_{n_tr} \cdot 4 \cdot 50 \cdot \text{per} \quad n := 0 .. n_f \quad t_f := .02 \cdot \text{per} \quad t := 0, \frac{t_f}{n_f} .. t_f$$



Las corrientes se pueden escribir como,

$$i_{ia}(t) = (s_1(t) - s_4(t)) \cdot i_{dc}(t)$$

$$i_{ib}(t) = (s_3(t) - s_6(t)) \cdot i_{dc}(t)$$

$$i_{ic}(t) = (s_5(t) - s_2(t)) \cdot i_{dc}(t)$$

Se define la función de conmutación como,

$$s_a(t) := s_1(t) - s_4(t)$$

$$s_b(t) := s_3(t) - s_6(t)$$

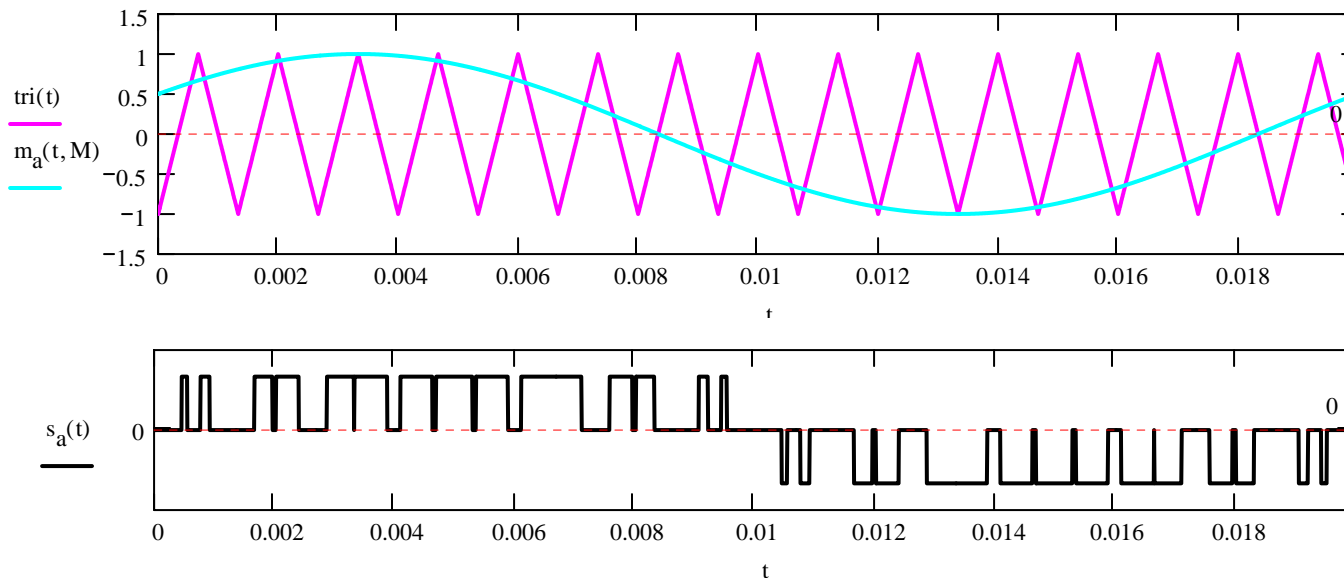
$$s_c(t) := s_5(t) - s_2(t)$$

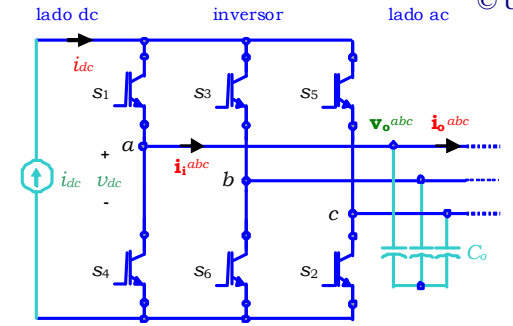
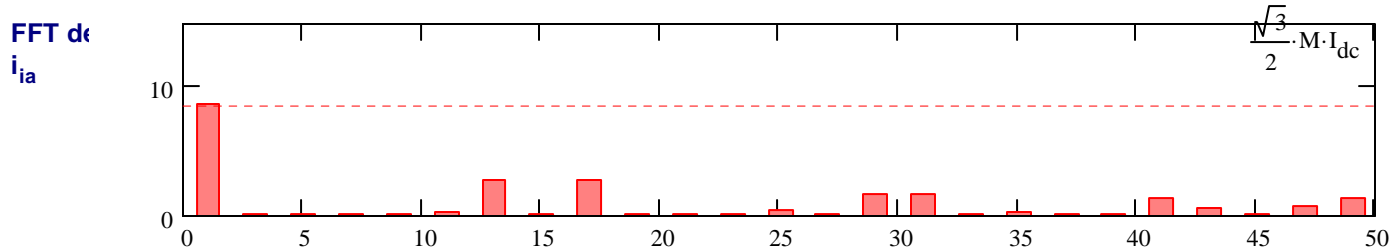
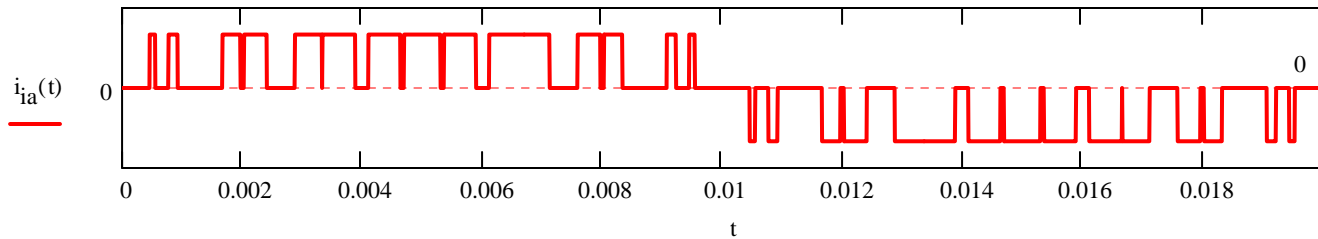
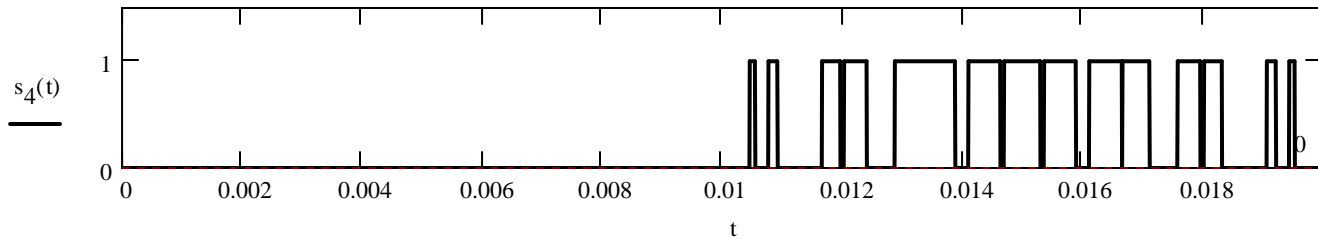
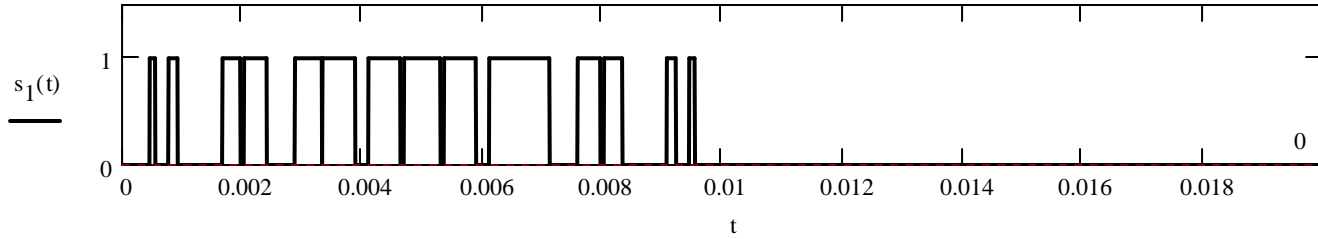
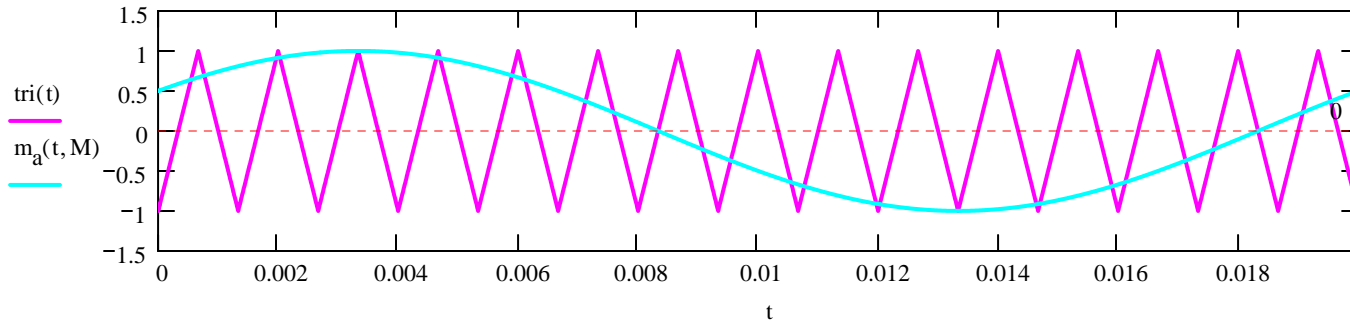
$$i_{ia}(t) = s_a(t) \cdot i_{dc}(t)$$

$$i_{ib}(t) = s_b(t) \cdot i_{dc}(t)$$

$$i_{ic}(t) = s_c(t) \cdot i_{dc}(t)$$

Hay un desfase entre la moduladora y la señal de conmutación.





$$s_a(t) := s_1(t) - s_4(t)$$

$$I_{dc} := 10$$

$$i_{dc}(t) := I_{dc}$$

$$i_{ia}(t) := s_a(t) \cdot i_{dc}(t)$$

Hay un desfase entre la moduladora y la señal de conmutación.

$N := 1024$

$m := 1 \dots N$

$$x_m := i_{ia}\left(\frac{m}{N} \cdot t_f\right)$$

$xf := \text{FFT}(x)$

$$xv(m) := \text{if}(m = 1, 1, 2) \cdot xf_{m\text{-per}}$$

$$|xv(2)| = 8.602 \quad \frac{\sqrt{3}}{2} \cdot M \cdot I_{dc} = 8.66$$

La fundamental de la corriente ac es igual a $0.866MI_{dc}$ y no hay componentes de frecuencia hasta $f_{n_tr} / 2$.

La moduladora es, $M := 1 \quad \omega_s := 2 \cdot \pi \cdot 50 \quad f_M := 0$

La triangular es, $f_{n_tr} := 15 \text{ per} := 1$

$$tri(t) := \frac{2}{\pi} \cdot asin \left(\sin \left(f_{n_tr} \cdot \omega_s \cdot t + f_M \cdot f_{n_tr} - \frac{\pi}{2} \right) \right)$$

$$m_a(t, M) := M \cdot \sin \left(\omega_s \cdot t + f_M - \frac{0 \cdot \pi}{3} \right)$$

$$m_b(t, M) := M \cdot \sin \left(\omega_s \cdot t + f_M - \frac{2 \cdot \pi}{3} \right)$$

$$m_c(t, M) := M \cdot \sin \left(\omega_s \cdot t + f_M - \frac{4 \cdot \pi}{3} \right)$$

Auxiliar 1 $m_{ax}(t, M) := (m_a(t, M) - m_b(t, M)) \cdot (\sqrt{3})^{-1}$

$$s_x(t) := \text{if}(m_{ax}(t, M) > tri(t), 1, 0)$$

$$s_{xn}(t) := \text{if}(s_x(t) = 1, 0, 1)$$

Auxiliar 2 $m_{bx}(t, M) := (m_b(t, M) - m_c(t, M)) \cdot (\sqrt{3})^{-1}$

$$s_y(t) := \text{if}(m_{bx}(t, M) > tri(t), 1, 0)$$

$$s_{yn}(t) := \text{if}(s_y(t) = 1, 0, 1)$$

Auxiliar 3 $m_{cx}(t, M) := (m_c(t, M) - m_a(t, M)) \cdot (\sqrt{3})^{-1}$

$$s_z(t) := \text{if}(m_{cx}(t, M) > tri(t), 1, 0)$$

$$s_{zn}(t) := \text{if}(s_z(t) = 1, 0, 1)$$

1ra pierna $s_1(t) := s_x(t) \cdot s_{zn}(t)$

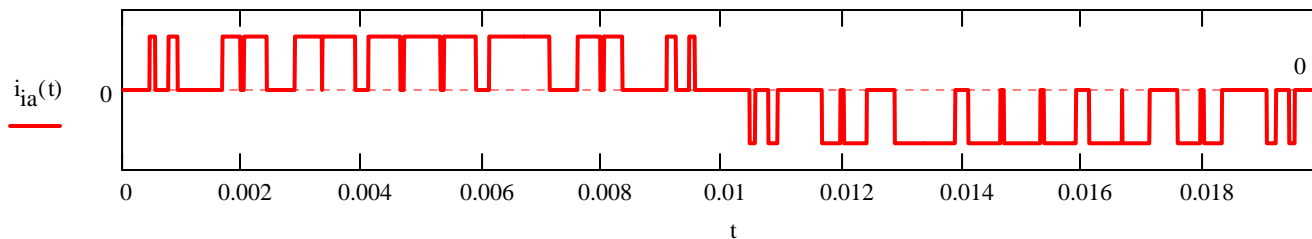
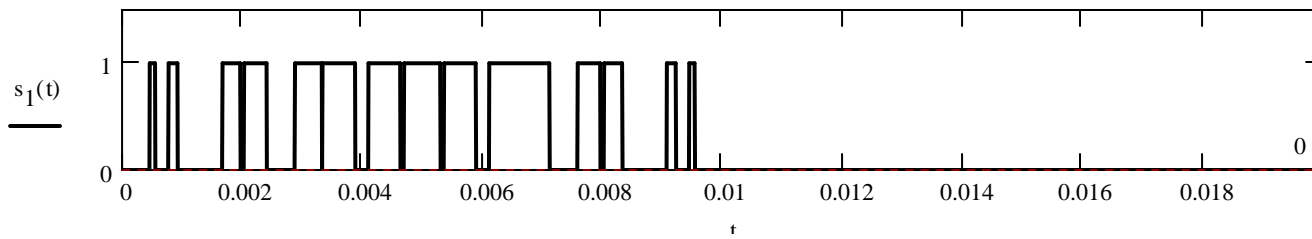
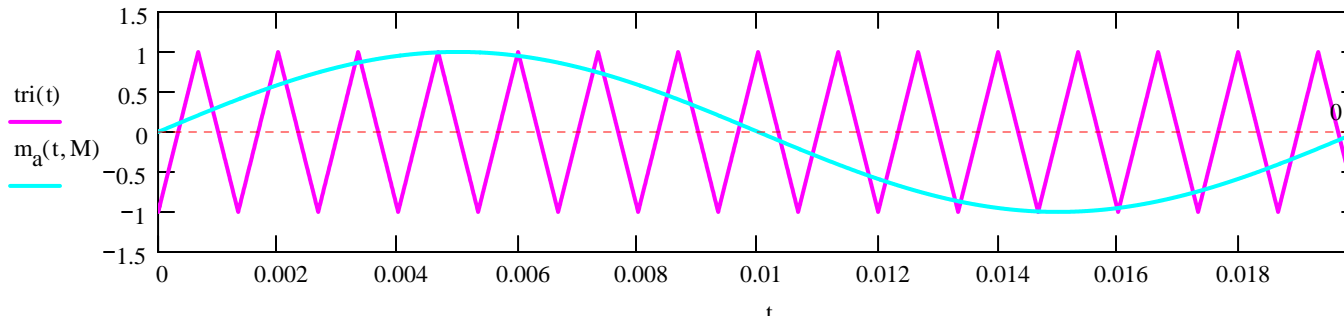
$$s_4(t) := s_z(t) \cdot s_{xn}(t)$$

2da pierna $s_3(t) := s_y(t) \cdot s_{xn}(t)$

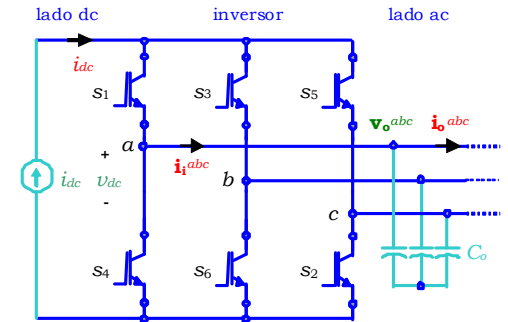
$$s_6(t) := s_x(t) \cdot s_{yn}(t)$$

3ra pierna $s_5(t) := s_z(t) \cdot s_{yn}(t)$

$$s_2(t) := s_y(t) \cdot s_{zn}(t)$$



Hay un desfase entre la moduladora y la señal de conmutación que se corrige con las señales auxiliares m_{ax} , m_{bx} y m_{cx} .



$$s_a(t) := s_1(t) - s_4(t)$$

$$s_b(t) := s_3(t) - s_6(t)$$

$$s_c(t) := s_5(t) - s_2(t)$$

$$I_{dc} := 10$$

$$i_{dc}(t) := I_{dc}$$

$$i_{ia}(t) := s_a(t) \cdot i_{dc}(t)$$

Modelo de Inversor de Corriente Trifásico

Problema Estudiar el modelo del inversor de corriente con Modulación SPWM.

La suma de las corrientes de carga es cero y la carga es balanceada, entonces,

$$v_{o_an}(t) + v_{o_bn}(t) + v_{o_cn}(t) = 0$$

$$v_{o_an}(t) = R_o \cdot i_{o_a}(t) + L_o \cdot di_{o_a}(t)$$

$$v_{o_bn}(t) = R_o \cdot i_{o_b}(t) + L_o \cdot di_{o_b}(t)$$

$$v_{o_cn}(t) = R_o \cdot i_{o_c}(t) + L_o \cdot di_{o_c}(t)$$

$$v_{o_n}(t) = R_o \cdot i_o(t) + L_o \cdot di_o(t)$$

$$s_i(t) \cdot i_{dc}(t) = C_o \cdot dv_{o_n}(t) + i_o(t)$$

$$di_o(t) = \frac{-R_o}{L_o} \cdot i_o(t) + \frac{1}{L_o} \cdot v_{o_n}(t) \quad dv_{o_n}(t) = \frac{-1}{C_o} \cdot i_o(t) + \frac{1}{C_o} \cdot s_i(t) \cdot i_{dc}(t)$$

$$i_{i_a}(t) = s_a(t) \cdot i_{dc}(t) = (s_1(t) - s_4(t)) \cdot i_{dc}(t)$$

$$i_{i_b}(t) = s_b(t) \cdot i_{dc}(t) = (s_3(t) - s_6(t)) \cdot i_{dc}(t)$$

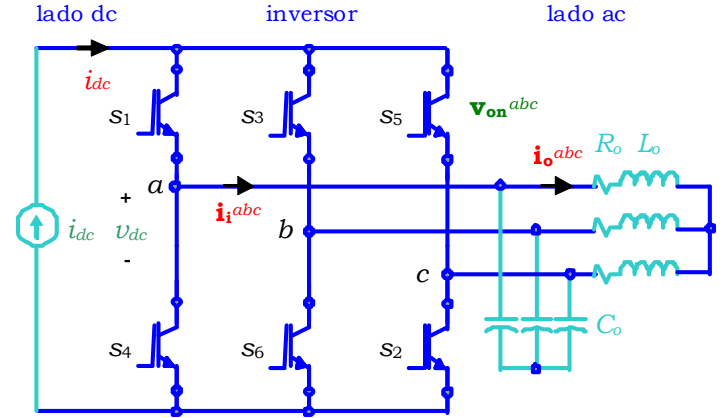
$$i_{i_c}(t) = s_c(t) \cdot i_{dc}(t) = (s_5(t) - s_2(t)) \cdot i_{dc}(t)$$

$$i_{i_a}(t) = C_o \cdot dv_{o_an}(t) + i_{o_a}(t)$$

$$i_{i_b}(t) = C_o \cdot dv_{o_bn}(t) + i_{o_b}(t)$$

$$i_{i_c}(t) = C_o \cdot dv_{o_cn}(t) + i_{o_c}(t)$$

$$s_i(t) := \begin{pmatrix} s_a(t) \\ s_b(t) \\ s_c(t) \end{pmatrix}$$



$$v_{dc}(t) \cdot i_{dc}(t) = v_{o_n}(t)^T \cdot i_i(t)$$

$$i_i(t) = s_i(t) \cdot i_{dc}(t)$$

$$v_{dc}(t) \cdot i_{dc}(t) = v_{o_n}(t)^T \cdot s_i(t) \cdot i_{dc}(t)$$

$$v_{dc}(t) = v_{o_n}(t)^T \cdot s_i(t)$$

$$v_{dc}(t) = v_{o_n}(t)^T \cdot s_i(t)$$

Parámetros

$$L_o := 15 \cdot 10^{-3} \quad R_o := 10 \quad C_o := 100 \cdot 10^{-6} \quad i_{dc}(t) := I_{dc}$$

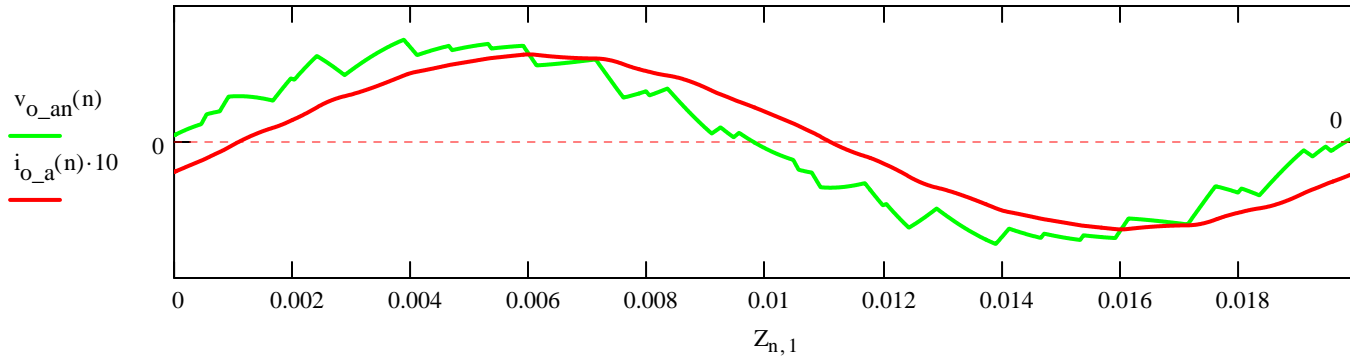
Simulación $t_f := 0.02$ $n_f := 2048$ $n := 1 .. n_f$ $t := 0, \frac{t_f}{n_f} .. t_f$

$$D(t, x) := \text{stack} \left(\frac{-R_o}{L_o} \cdot (x_1 \ x_2 \ x_3)^T + \frac{1}{L_o} \cdot (x_4 \ x_5 \ x_6)^T, \frac{-1}{C_o} \cdot (x_1 \ x_2 \ x_3)^T + \frac{1}{C_o} \cdot s_i(t) \cdot i_{dc}(t) \right) \quad CI := \text{stack} \left(\begin{pmatrix} 0 \\ 0 \\ 0 \end{pmatrix}, \begin{pmatrix} 0 \\ 0 \\ 0 \end{pmatrix} \right) \quad Z := \text{rkfixed}(CI, 0, t_f, n_f, D)$$

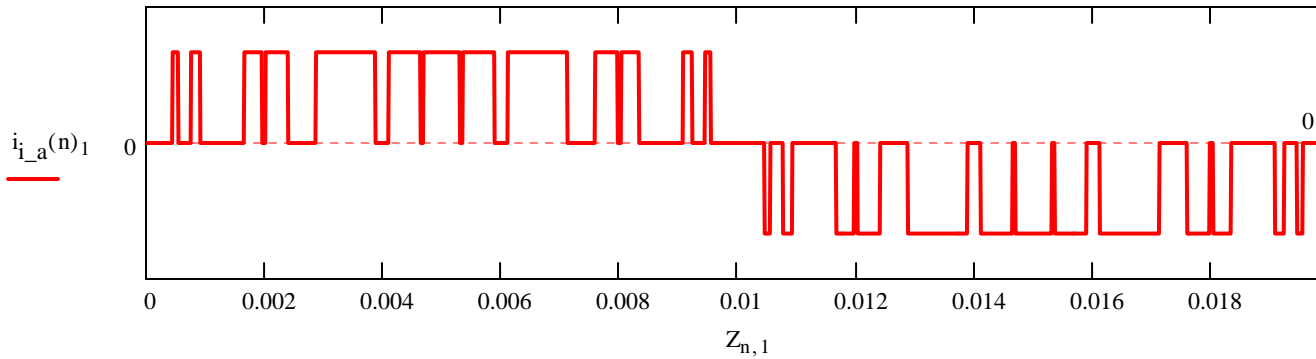
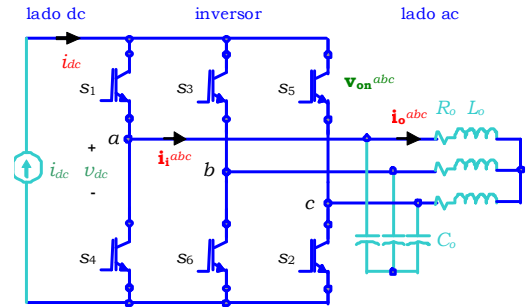
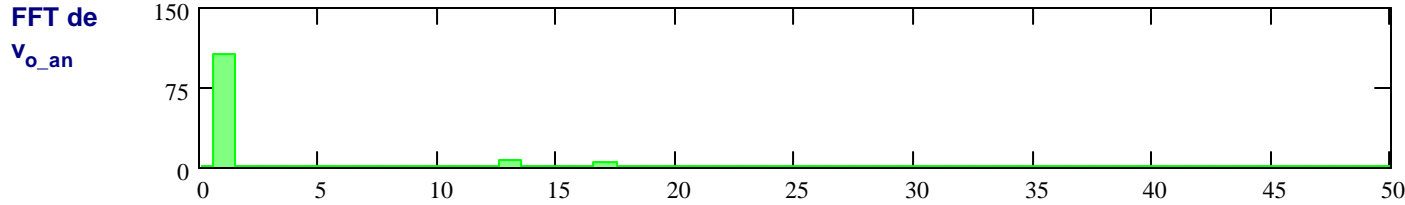
$$CI := \text{stack} \left((Z_{n_f, 2} \ Z_{n_f, 3} \ Z_{n_f, 4})^T, (Z_{n_f, 5} \ Z_{n_f, 6} \ Z_{n_f, 7})^T \right) \quad Z := \text{rkfixed}(CI, 0, t_f, n_f, D)$$

$$v_{o_an}(n) := Z_{n,5} \quad v_{o_bn}(n) := Z_{n,6} \quad v_{o_cn}(n) := Z_{n,7} \quad i_{i_a}(n) := s_i \left(n \cdot \frac{t_f}{n_f} \right) \cdot i_{dc} \left(n \cdot \frac{t_f}{n_f} \right)$$

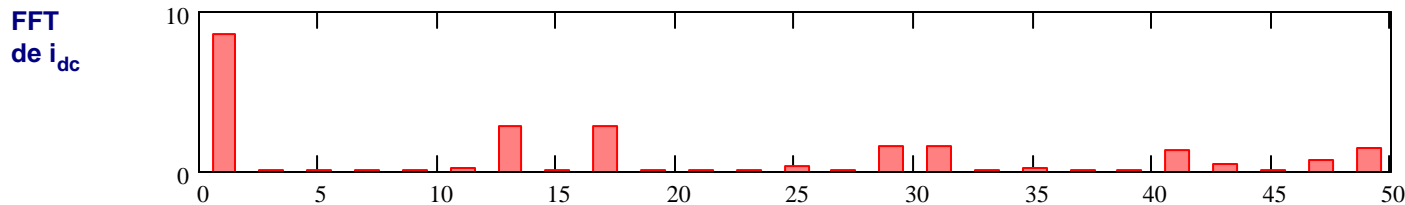
$$i_{o_a}(n) := Z_{n,2} \quad i_{o_b}(n) := Z_{n,3} \quad i_{o_c}(n) := Z_{n,4} \quad v_{dc}(n) := \left(v_{o_an}(n) \ v_{o_bn}(n) \ v_{o_cn}(n) \right)^T \cdot s_i \left(n \cdot \frac{t_f}{n_f} \right)$$



```
N := 1024      m := 1..N
x_m := v_o_an(m/N * n_f)  xf := FFT(x)
xv(m) := if(m = 1, 1, 2) * xf_m_per
|xv(2)| = 105.242
```



```
N := 1024      m := 1..N
x_m := i_i_a(m/N * n_f)_1  xf := FFT(x)
xv(m) := if(m = 1, 1, 2) * xf_m_per
|xv(2)| = 8.602
```



$$\frac{\sqrt{3}}{2} \cdot M \cdot I_{dc} = 8.66$$

La fundamental de la corriente ac es igual a $0.866MI_{dc}$ y están en fase.

Modelo Promedio de Inversor de Corriente Trifásico

Problema Estudiar el modelo promedio del inversor de corriente.

Se utiliza la relación entre la fundamental de corriente y la moduladora.

$$\begin{pmatrix} i_{i_a}(t) \\ i_{i_b}(t) \\ i_{i_c}(t) \end{pmatrix} = \frac{\sqrt{3}}{2} \cdot \begin{pmatrix} m_a(t) \\ m_b(t) \\ m_c(t) \end{pmatrix} \cdot i_{dc}(t)$$

$$v_{o_an}(t) = R_o \cdot i_{o_a}(t) + L_o \cdot di_{o_a}(t)$$

$$i_{i_a}(t) = C_o \cdot dv_{o_an}(t) + i_{o_a}(t)$$

$$v_{o_bn}(t) = R_o \cdot i_{o_b}(t) + L_o \cdot di_{o_b}(t)$$

$$i_{i_b}(t) = C_o \cdot dv_{o_bn}(t) + i_{o_b}(t)$$

$$v_{o_cn}(t) = R_o \cdot i_{o_c}(t) + L_o \cdot di_{o_c}(t)$$

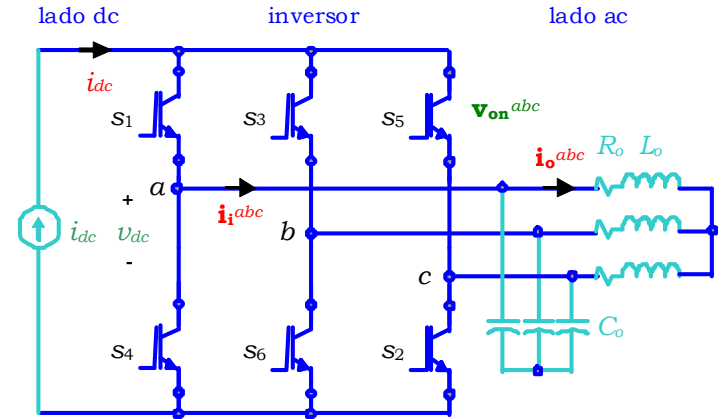
$$i_{i_c}(t) = C_o \cdot dv_{o_cn}(t) + i_{o_c}(t)$$

$$v_{o_n}(t) = R_o \cdot i_o(t) + L_o \cdot di_o(t)$$

$$m_i(t) := \frac{\sqrt{3}}{2} \begin{pmatrix} m_a(t, M) \\ m_b(t, M) \\ m_c(t, M) \end{pmatrix}$$

$$m_i(t) \cdot i_{dc}(t) = C_o \cdot dv_{o_n}(t) + i_o(t)$$

$$di_o(t) = \frac{-R_o}{L_o} \cdot i_o(t) + \frac{1}{L_o} \cdot v_{o_n}(t) \quad dv_{o_n}(t) = \frac{-1}{C_o} \cdot i_o(t) + \frac{1}{C_o} \cdot m_i(t) \cdot i_{dc}(t)$$



$$v_{dc}(t) \cdot i_{dc}(t) = v_{o_n}(t)^T \cdot i_i(t)$$

$$i_i(t) = m_i(t) \cdot i_{dc}(t)$$

$$v_{dc}(t) \cdot i_{dc}(t) = v_{o_n}(t)^T \cdot m_i(t) \cdot i_{dc}(t)$$

$$v_{dc}(t) = v_{o_n}(t)^T \cdot m_i(t)$$

$$v_{dc}(t) = v_{o_n}(t)^T \cdot m_i(t)$$

Parámetros

$$L_o := 15 \cdot 10^{-3} \quad R_o := 10 \quad C_o := 100 \cdot 10^{-6} \quad i_{dc}(t) := I_{dc}$$

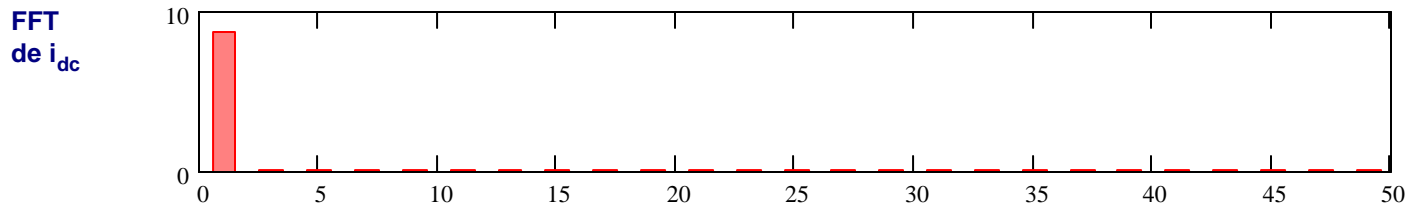
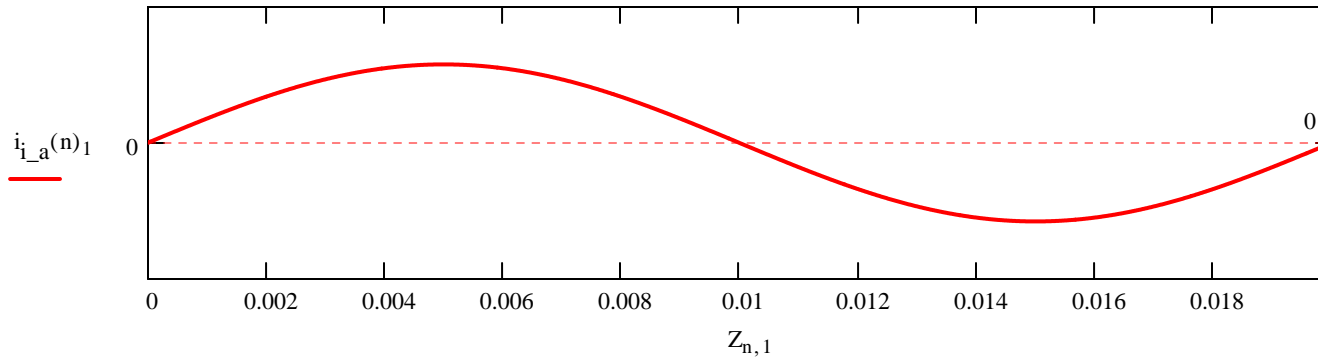
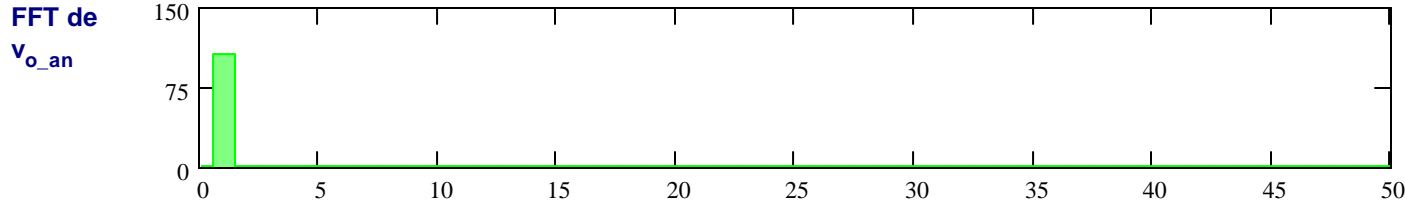
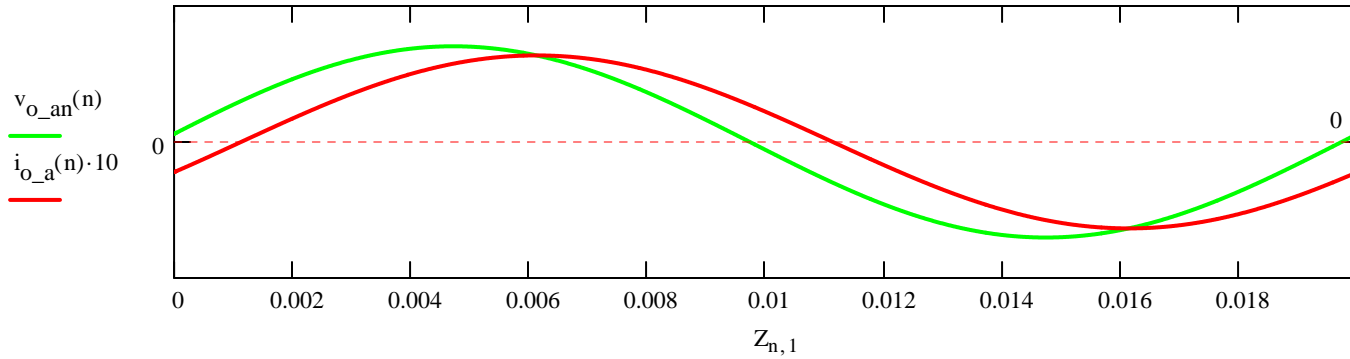
Simulación $t_f := 0.02$ $n_f := 2048$ $n := 1 \dots n_f$ $t := 0, \frac{t_f}{n_f} \dots t_f$

$$D(t, x) := \text{stack} \left(\frac{-R_o}{L_o} \cdot (x_1 \ x_2 \ x_3)^T + \frac{1}{L_o} \cdot (x_4 \ x_5 \ x_6)^T, \frac{-1}{C_o} \cdot (x_1 \ x_2 \ x_3)^T + \frac{1}{C_o} \cdot m_i(t) \cdot i_{dc}(t) \right) \quad CI := \text{stack} \left(\begin{pmatrix} 0 \\ 0 \\ 0 \end{pmatrix}, \begin{pmatrix} 0 \\ 0 \\ 0 \end{pmatrix} \right) \quad Z := \text{rkfixed}(CI, 0, t_f, n_f, D)$$

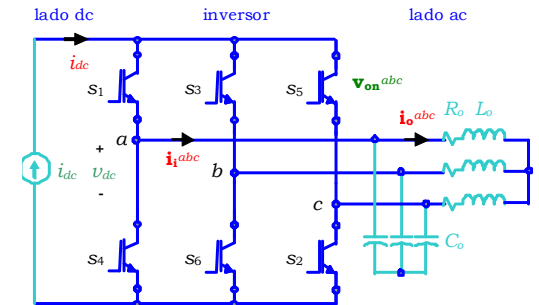
$$CI := \text{stack} \left((Z_{n_f, 2} \ Z_{n_f, 3} \ Z_{n_f, 4})^T, (Z_{n_f, 5} \ Z_{n_f, 6} \ Z_{n_f, 7})^T \right) \quad Z := \text{rkfixed}(CI, 0, t_f, n_f, D)$$

$$v_{o_an}(n) := Z_{n,5} \quad v_{o_bn}(n) := Z_{n,6} \quad v_{o_cn}(n) := Z_{n,7} \quad i_{i_a}(n) := m_i \left(n \cdot \frac{t_f}{n_f} \right) \cdot i_{dc} \left(n \cdot \frac{t_f}{n_f} \right)$$

$$i_{o_a}(n) := Z_{n,2} \quad i_{o_b}(n) := Z_{n,3} \quad i_{o_c}(n) := Z_{n,4} \quad v_{dc}(n) := \left(v_{o_an}(n) \ v_{o_bn}(n) \ v_{o_cn}(n) \right)^T \cdot m_i \left(n \cdot \frac{t_f}{n_f} \right)$$



```
N := 1024      m := 1..N
x_m := v_o_an(m/N * n_f)  xf := FFT(x)
xv(m) := if(m = 1, 1, 2) * xf_m_per
|xv(2)| = 105.456
```



```
N := 1024      m := 1..N
x_m := i_i_a(m/N * n_f)_1  xf := FFT(x)
xv(m) := if(m = 1, 1, 2) * xf_m_per
|xv(2)| = 8.66
```

$$\frac{\sqrt{3}}{2} \cdot M \cdot I_{dc} = 8.66$$

La fundamental de la corriente ac es igual a $0.866MI_{dc}$ y están en fase.

Modelo de Rectificador de Corriente Trifásico

Problema Estudiar el modelo del rectificador de corriente con Modulación SPWM.

$$i_{r_a}(t) = s_a(t) \cdot i_{dc}(t) = (s_1(t) - s_4(t)) \cdot i_{dc}(t)$$

$$i_{r_b}(t) = s_b(t) \cdot i_{dc}(t) = (s_3(t) - s_6(t)) \cdot i_{dc}(t)$$

$$i_{r_c}(t) = s_c(t) \cdot i_{dc}(t) = (s_5(t) - s_2(t)) \cdot i_{dc}(t)$$

$$v_{s_a}(t) = R_s \cdot i_{s_a}(t) + L_s \cdot di_{s_a}(t) + v_{r_an}(t)$$

$$v_{s_b}(t) = R_s \cdot i_{s_b}(t) + L_s \cdot di_{s_b}(t) + v_{r_bn}(t)$$

$$v_{s_c}(t) = R_s \cdot i_{s_c}(t) + L_s \cdot di_{s_c}(t) + v_{r_cn}(t)$$

$$i_{s_a}(t) = i_{r_a}(t) + C_r \cdot dv_{r_an}(t)$$

$$i_{s_b}(t) = i_{r_b}(t) + C_r \cdot dv_{r_bn}(t)$$

$$i_{s_c}(t) = i_{r_c}(t) + C_r \cdot dv_{r_cn}(t)$$

$$v_{dc}(t) = L_{dc} \cdot di_{dc}(t) + R_{dc} \cdot i_{dc}(t)$$

$$v_s(t) := \left(\sqrt{2} \cdot 220 \cdot \sin(\omega_s \cdot t) \quad \sqrt{2} \cdot 220 \cdot \sin\left(\omega_s \cdot t - 2 \cdot \frac{\pi}{3}\right) \quad \sqrt{2} \cdot 220 \cdot \sin\left(\omega_s \cdot t - 4 \cdot \frac{\pi}{3}\right) \right)^T$$

Parámetros

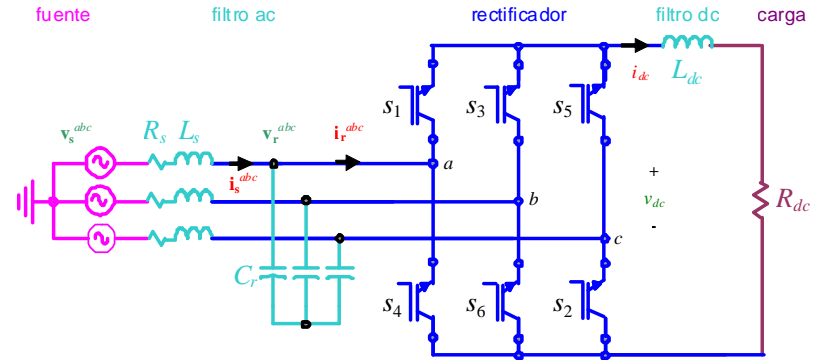
$$L_s := 30 \cdot 10^{-3}$$

$$R_s := 1$$

$$C_r := 50 \cdot 10^{-6}$$

$$R_{dc} := 10$$

$$L_{dc} := 30 \cdot 10^{-3}$$



$$v_{dc}(t) \cdot i_{dc}(t) = v_{r_n}(t)^T \cdot i_r(t)$$

$$i_r(t) = s_r(t) \cdot i_{dc}(t)$$

$$v_{dc}(t) \cdot i_{dc}(t) = v_{r_n}(t)^T \cdot s_r(t) \cdot i_{dc}(t)$$

$$v_{dc}(t) = v_{r_n}(t)^T \cdot s_r(t)$$

$$v_{dc}(t) = v_{r_n}(t)^T \cdot s_r(t)$$

$$s_r(t) := s_i(t)$$

$$v_s(t) = R_s \cdot i_s(t) + L_s \cdot di_s(t) + v_{r_n}(t)$$

$$i_s(t) = C_r \cdot dv_{r_n}(t) + s_r(t) \cdot i_{dc}(t)$$

$$v_{r_n}(t)^T \cdot s_r(t) = L_{dc} \cdot di_{dc}(t) + R_{dc} \cdot i_{dc}(t)$$

$$di_s(t) = \frac{-R_s}{L_s} \cdot i_s(t) - \frac{1}{L_s} \cdot v_{r_n}(t) + \frac{1}{L_s} \cdot v_s(t)$$

$$dv_{r_n}(t) = \frac{-1}{C_r} \cdot s_r(t) \cdot i_{dc}(t) + \frac{1}{C_r} \cdot i_s(t)$$

$$di_{dc}(t) = \frac{-R_{dc}}{L_{dc}} \cdot i_{dc}(t) + \frac{1}{L_{dc}} \cdot v_{r_n}(t)^T \cdot s_r(t)$$

Simulación $t_f := 0.02$ $n_f := 2048$ $n := 1 .. n_f$ $t := 0, \frac{t_f}{n_f} .. t_f$

$$D(t, x) := \text{stack} \left(\frac{-R_s}{L_s} \cdot (x_1 \ x_2 \ x_3)^T - \frac{1}{L_s} \cdot (x_4 \ x_5 \ x_6)^T + \frac{1}{L_s} \cdot v_s(t), \frac{-1}{C_r} \cdot s_r(t) \cdot x_7 + \frac{1}{C_r} \cdot (x_1 \ x_2 \ x_3)^T, \frac{-R_{dc}}{L_{dc}} \cdot x_7 + \frac{1}{L_{dc}} \cdot (x_4 \ x_5 \ x_6)^T \cdot s_r(t) \right)$$

$$CI := (5.537 \quad -38.684 \quad 33.281 \quad -371.682 \quad -81.54 \quad 490.274 \quad 43.18)^T$$

$$Z := \text{rkfixed}(CI, 0, t_f, n_f, D)$$

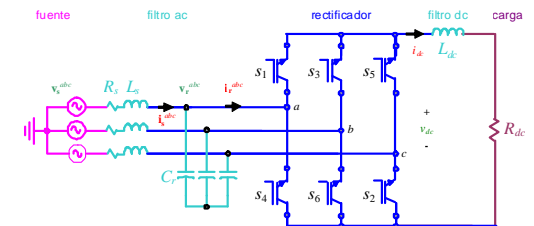
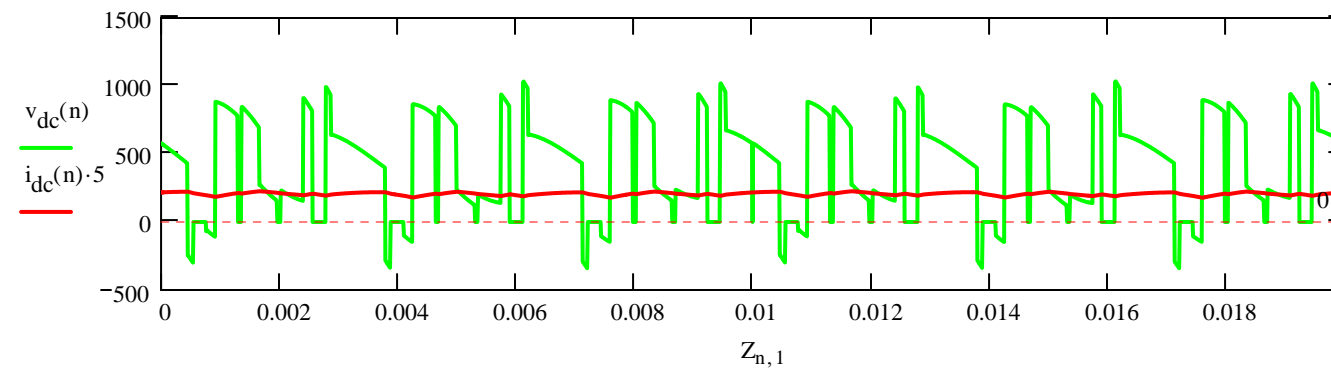
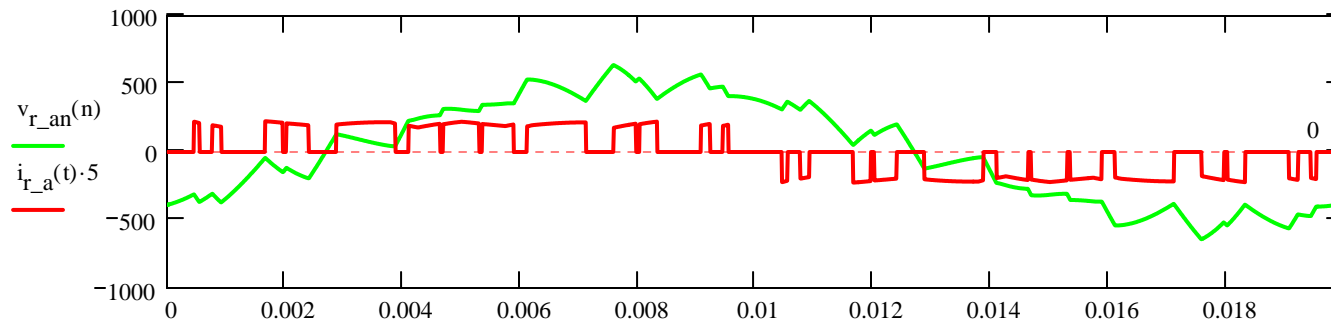
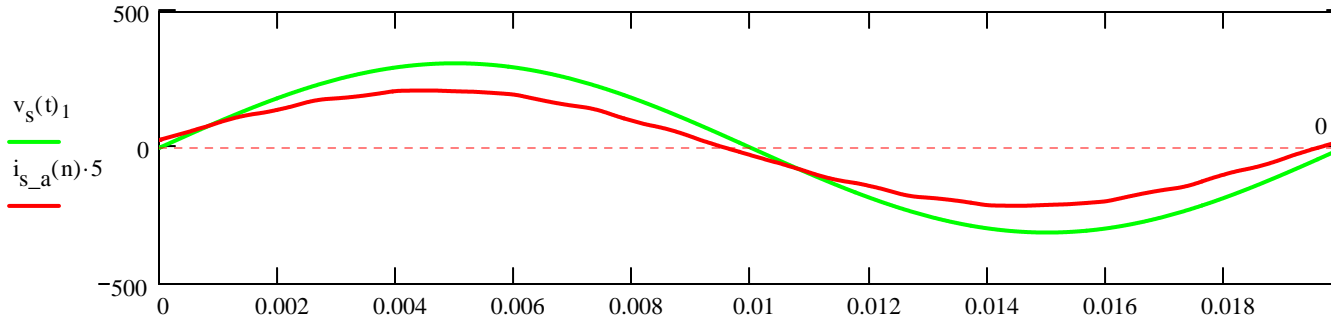
$$CI := \left(Z_{n_f, 2} \quad Z_{n_f, 3} \quad Z_{n_f, 4} \quad Z_{n_f, 5} \quad Z_{n_f, 6} \quad Z_{n_f, 7} \quad Z_{n_f, 8} \right)^T$$

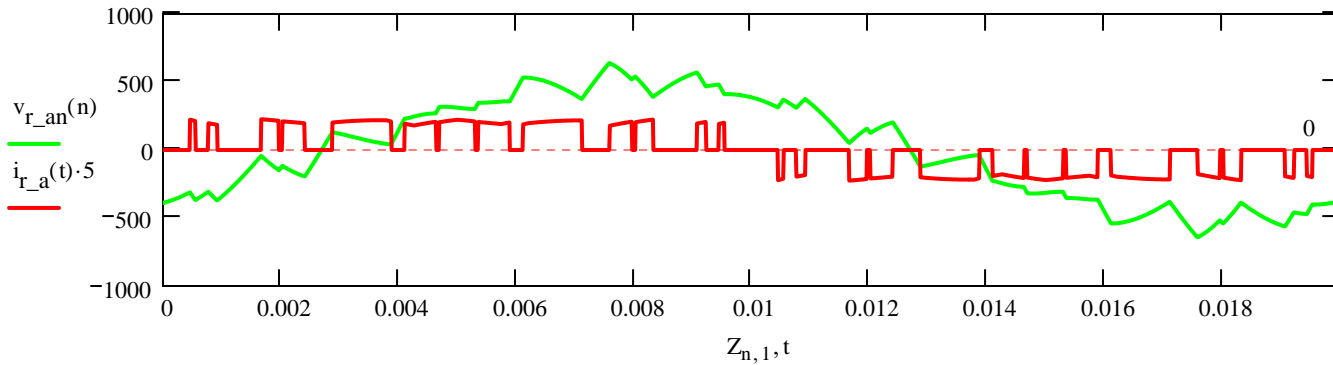
$$Z := \text{rkfixed}(CI, 0, t_f, n_f, D)$$

$$i_{dc}(n) := Z_{n,8} \quad i_{r_a}(t) := \left(s_r(t) \cdot i_{dc} \left(t \cdot \frac{n_f}{t_f} \right) \right)_1 \quad i_{r_b}(t) := \left(s_r(t) \cdot i_{dc} \left(t \cdot \frac{n_f}{t_f} \right) \right)_2 \quad i_{r_c}(t) := \left(s_r(t) \cdot i_{dc} \left(t \cdot \frac{n_f}{t_f} \right) \right)_3$$

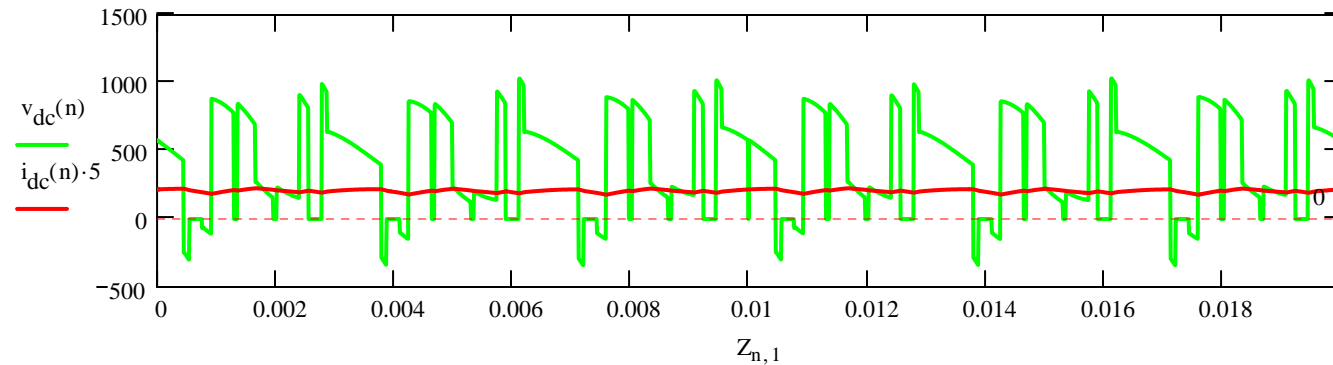
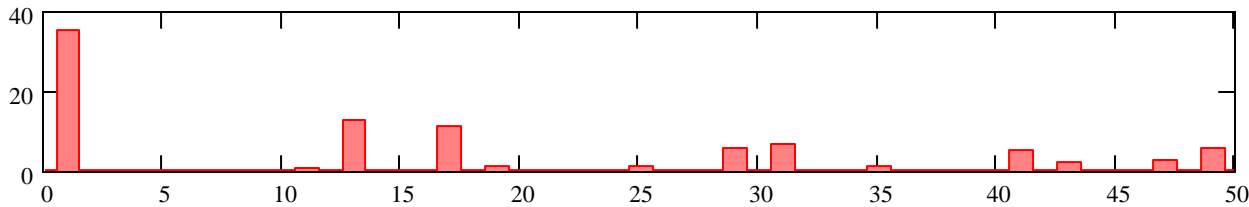
$$i_{s_a}(n) := Z_{n,2} \quad i_{s_b}(n) := Z_{n,3} \quad i_{s_c}(n) := Z_{n,4} \quad v_{r_an}(n) := Z_{n,5} \quad v_{r_bn}(n) := Z_{n,6} \quad v_{r_cn}(n) := Z_{n,7}$$

$$v_{dc}(n) := s_r \left(n \cdot \frac{t_f}{n_f} \right)^T \cdot \left(v_{r_an}(n) \quad v_{r_bn}(n) \quad v_{r_cn}(n) \right)^T$$

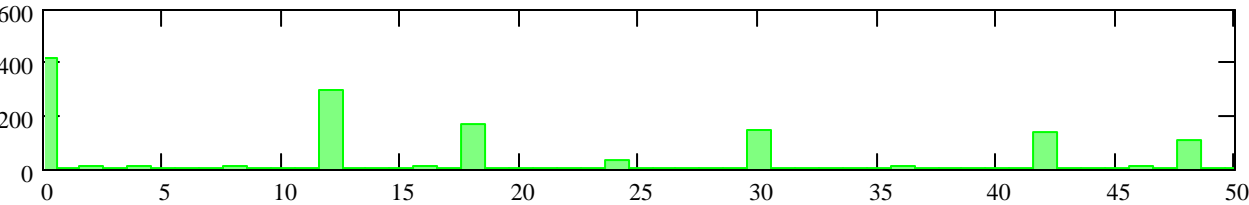




FFT de i_{r_a}



FFT de v_{dc}



$$N := 1024 \quad m := 1..N$$

$$x_m := i_{r_a}\left(\frac{m}{N} \cdot t_f\right) \quad xf := \text{FFT}(x)$$

$$xv(m) := \text{if}(m = 1, 1, 2) \cdot xf_{m_per}$$

$$|xv(2)| = 35.445$$

$$\frac{\sqrt{3}}{2} \cdot M \cdot i_{dc}(1) = 37.524$$

La fundamental de corriente es igual a 0.866 M I_{dc}

$$N := 1024 \quad m := 1..N$$

$$x_m := v_{dc}\left(\frac{m}{N} \cdot n_f\right) \quad xf := \text{FFT}(x)$$

$$xv(m) := \text{if}(m = 1, 1, 2) \cdot xf_{m_per}$$

$$|xv(1)| = 413.522 \quad V_{dc} := |xv(1)|$$

$$P_o := \frac{V_{dc}^2}{R_{dc}} \quad P_o = 1.71 \times 10^4$$

El voltaje DC no tiene segunda armónica. Sólo armónicas de conmutación.

Modelo Promedio de Rectificador de Corriente Trifásico

Problema Estudiar el modelo promedio del rectificador de corriente.

$$\begin{pmatrix} i_{r_a}(t) \\ i_{r_b}(t) \\ i_{r_c}(t) \end{pmatrix} = \frac{\sqrt{3}}{2} \cdot \begin{pmatrix} m_a(t) \\ m_b(t) \\ m_c(t) \end{pmatrix} \cdot i_{dc}(t)$$

Parámetros

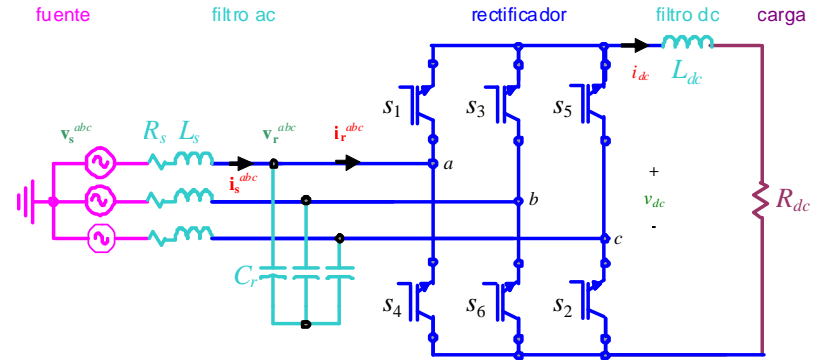
$$L_s := 30 \cdot 10^{-3}$$

$$R_s := 1$$

$$C_r := 50 \cdot 10^{-6}$$

$$R_{dc} := 10$$

$$L_{dc} := 30 \cdot 10^{-3}$$



$$v_{s_a}(t) = R_s \cdot i_{s_a}(t) + L_s \cdot di_{s_a}(t) + v_{r_an}(t)$$

$$v_{s_b}(t) = R_s \cdot i_{s_b}(t) + L_s \cdot di_{s_b}(t) + v_{r_bn}(t)$$

$$v_{s_c}(t) = R_s \cdot i_{s_c}(t) + L_s \cdot di_{s_c}(t) + v_{r_cn}(t)$$

$$i_{s_a}(t) = i_{r_a}(t) + C_r \cdot dv_{r_an}(t)$$

$$i_{s_b}(t) = i_{r_b}(t) + C_r \cdot dv_{r_bn}(t)$$

$$i_{s_c}(t) = i_{r_c}(t) + C_r \cdot dv_{r_cn}(t)$$

$$v_{dc}(t) = L_{dc} \cdot di_{dc}(t) + R_{dc} \cdot i_{dc}(t)$$

$$v_{dc}(t) \cdot i_{dc}(t) = v_{r_n}(t)^T \cdot i_r(t)$$

$$i_r(t) = m_r(t) \cdot i_{dc}(t)$$

$$v_{dc}(t) \cdot i_{dc}(t) = v_{r_n}(t)^T \cdot m_r(t) \cdot i_{dc}(t)$$

$$v_{dc}(t) = v_{r_n}(t)^T \cdot m_r(t)$$

$$v_{dc}(t) = v_{r_n}(t)^T \cdot m_r(t)$$

$$v_s(t) = R_s \cdot i_s(t) + L_s \cdot di_s(t) + v_{r_n}(t)$$

$$i_s(t) = C_r \cdot dv_{r_n}(t) + m_r(t) \cdot i_{dc}(t)$$

$$v_{r_n}(t)^T \cdot m_r(t) = L_{dc} \cdot di_{dc}(t) + R_{dc} \cdot i_{dc}(t)$$

$$di_s(t) = \frac{-R_s}{L_s} \cdot i_s(t) - \frac{1}{L_s} \cdot v_{r_n}(t) + \frac{1}{L_s} \cdot v_s(t)$$

$$dv_{r_n}(t) = \frac{-1}{C_r} \cdot m_r(t) \cdot i_{dc}(t) + \frac{1}{C_r} \cdot i_s(t)$$

$$di_{dc}(t) = \frac{-R_{dc}}{L_{dc}} \cdot i_{dc}(t) + \frac{1}{L_{dc}} \cdot v_{r_n}(t)^T \cdot m_r(t)$$

$$v_s(t) := \left(\sqrt{2} \cdot 220 \cdot \sin(\omega_s \cdot t) \quad \sqrt{2} \cdot 220 \cdot \sin\left(\omega_s \cdot t - 2 \cdot \frac{\pi}{3}\right) \quad \sqrt{2} \cdot 220 \cdot \sin\left(\omega_s \cdot t - 4 \cdot \frac{\pi}{3}\right) \right)^T$$

$$m_r(t) := \frac{\sqrt{3}}{2} \cdot \begin{pmatrix} m_a(t, M) \\ m_b(t, M) \\ m_c(t, M) \end{pmatrix}$$

Simulación $t_f := 0.02$ $n_f := 2048$ $n := 1 .. n_f$ $t := 0, \frac{t_f}{n_f} .. t_f$

$$D(t, x) := \text{stack} \left(\frac{-R_s}{L_s} \cdot (x_1 \ x_2 \ x_3)^T - \frac{1}{L_s} \cdot (x_4 \ x_5 \ x_6)^T + \frac{1}{L_s} \cdot v_s(t), \frac{-1}{C_r} \cdot m_r(t) \cdot x_7 + \frac{1}{C_r} \cdot (x_1 \ x_2 \ x_3)^T, \frac{-R_{dc}}{L_{dc}} \cdot x_7 + \frac{1}{L_{dc}} \cdot (x_4 \ x_5 \ x_6)^T \cdot m_r(t) \right)$$

$$CI := (4.868 \quad -38.653 \quad 33.835 \quad -398.658 \quad -69.957 \quad 475.516 \quad 41.046)^T$$

$$Z := \text{rkfixed}(CI, 0, t_f, n_f, D)$$

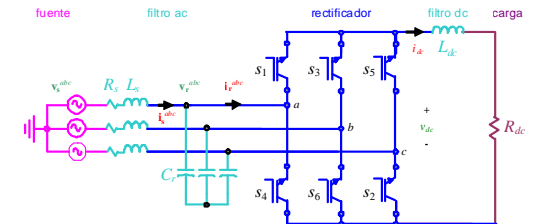
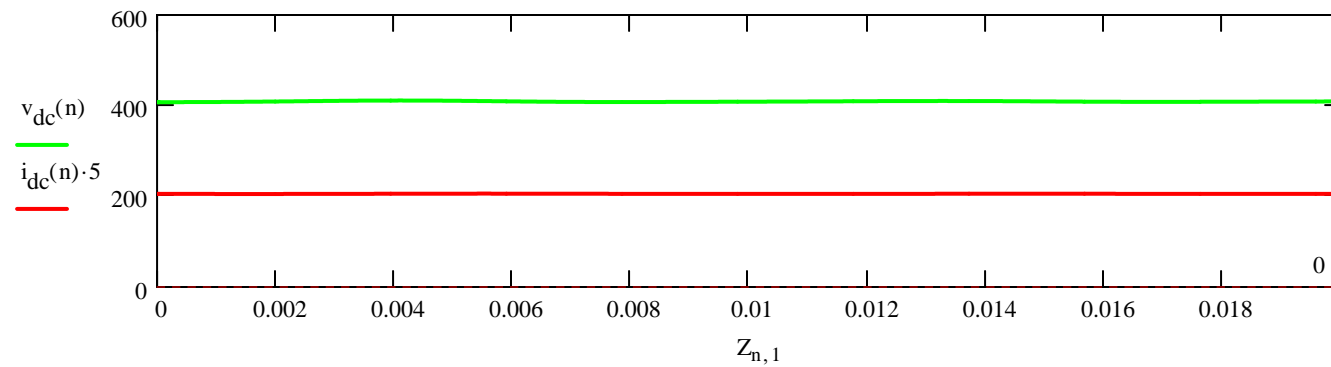
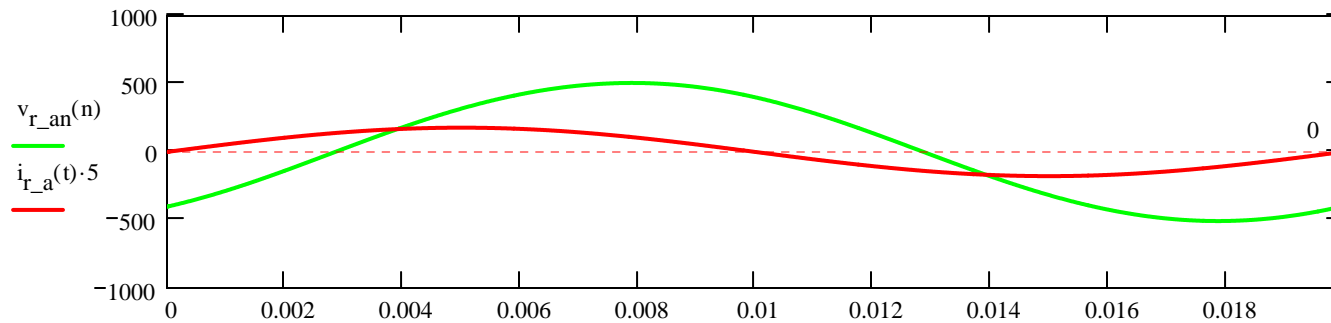
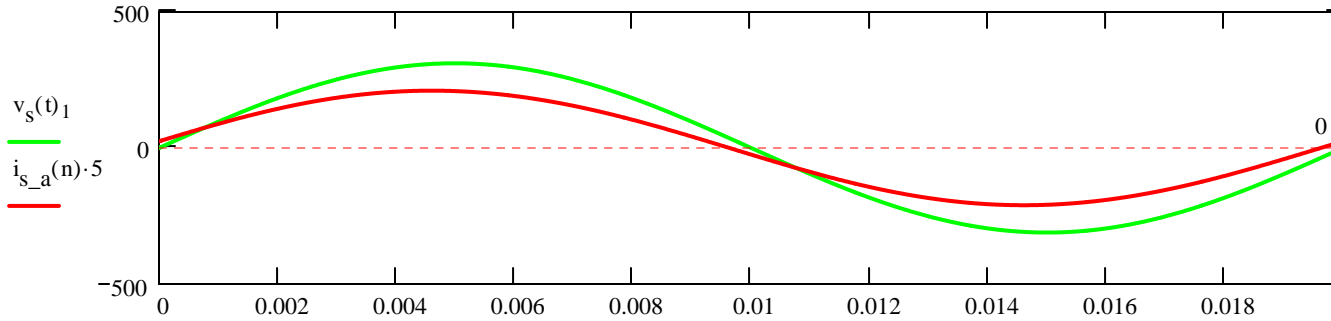
$$CI := \left(Z_{n_f,2} \quad Z_{n_f,3} \quad Z_{n_f,4} \quad Z_{n_f,5} \quad Z_{n_f,6} \quad Z_{n_f,7} \quad Z_{n_f,8} \right)^T$$

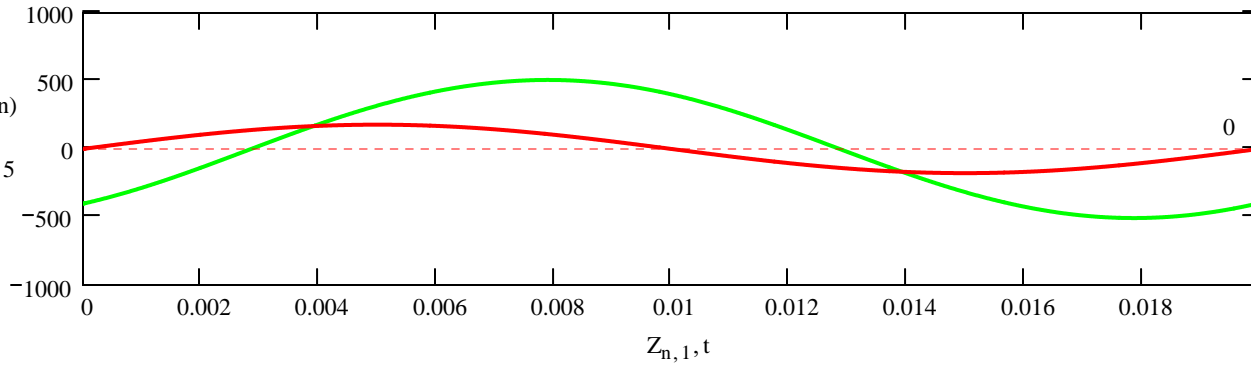
$$Z := \text{rkfixed}(CI, 0, t_f, n_f, D)$$

$$i_{dc}(n) := Z_{n,8} \quad i_{r_a}(t) := \left(m_r(t) \cdot i_{dc} \left(t \cdot \frac{n_f}{t_f} \right) \right)_1 \quad i_{r_b}(t) := \left(m_r(t) \cdot i_{dc} \left(t \cdot \frac{n_f}{t_f} \right) \right)_2 \quad i_{r_c}(t) := \left(m_r(t) \cdot i_{dc} \left(t \cdot \frac{n_f}{t_f} \right) \right)_3$$

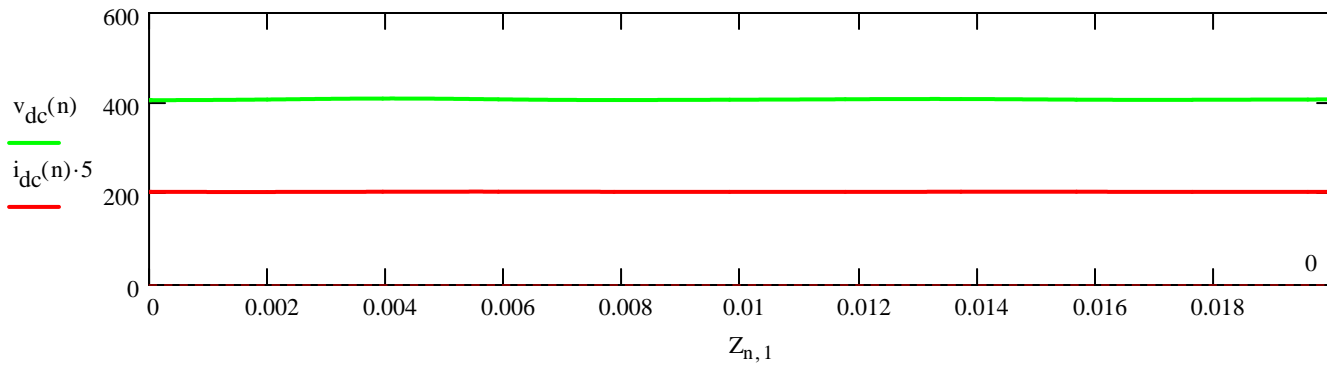
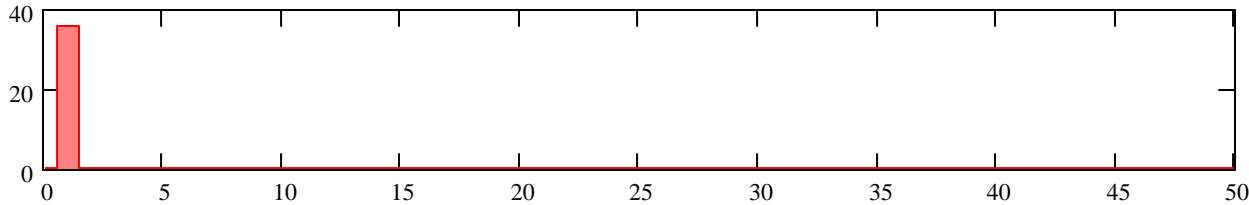
$$i_{s_a}(n) := Z_{n,2} \quad i_{s_b}(n) := Z_{n,3} \quad i_{s_c}(n) := Z_{n,4} \quad v_{r_an}(n) := Z_{n,5} \quad v_{r_bn}(n) := Z_{n,6} \quad v_{r_cn}(n) := Z_{n,7}$$

$$v_{dc}(n) := m_r \left(n \cdot \frac{t_f}{n_f} \right)^T \cdot (v_{r_an}(n) \quad v_{r_bn}(n) \quad v_{r_cn}(n))^T$$

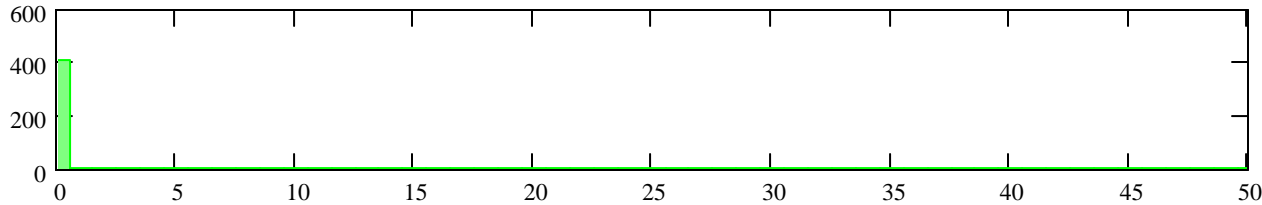




FFT de i_{r_a}



FFT de v_{dc}



$$N := 1024 \quad m := 1..N$$

$$x_m := i_{r_a}\left(\frac{m}{N} \cdot t_f\right) \quad xf := \text{FFT}(x)$$

$$xv(m) := \text{if}(m = 1, 1, 2) \cdot xv_{m_per}$$

$$|xv(2)| = 35.586$$

$$\frac{\sqrt{3}}{2} \cdot M \cdot i_{dc}(1) = 35.545$$

La fundamental de corriente es igual a $0.866 M I_{dc}$

$$N := 1024 \quad m := 1..N$$

$$x_m := v_{dc}\left(\frac{m}{N} \cdot n_f\right) \quad xf := \text{FFT}(x)$$

$$xv(m) := \text{if}(m = 1, 1, 2) \cdot xv_{m_per}$$

$$|xv(1)| = 409.071 \quad V_{dc} := |xv(1)|$$

$$P_o := \frac{V_{dc}^2}{R_{dc}} \quad P_o = 1.673 \times 10^4$$

El voltaje DC no tiene segunda armónica.

Modelo Promedio dq0 de Rectificador de Corriente Trifásico

Problema Estudiar el modelo promedio dq0 del rectificador de corriente.

$$\dot{i}_{rdq}(t) = m_{rdq}(t) \cdot i_{dc}(t)$$

$$v_{dc}(t) = v_{rdq_n}(t)^T \cdot m_{rdq}(t)$$

$$v_{sdq}(t) = R_s \cdot i_{sdq}(t) + L_s \cdot (di_{sdq}(t) + W \cdot i_{sdq}(t)) + v_{rdq_n}(t)$$

$$i_{sdq}(t) = C_r \cdot (dv_{rdq_n}(t) + W \cdot v_{rdq_n}(t)) + m_{rdq}(t) \cdot i_{dc}(t)$$

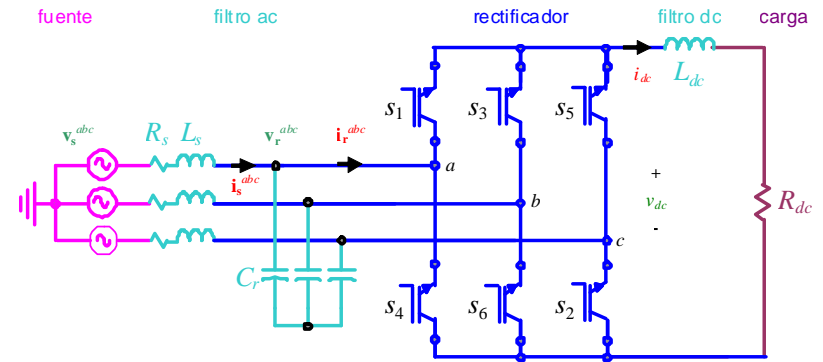
$$v_{rdq_n}(t)^T \cdot m_{rdq}(t) = L_{dc} \cdot di_{dc}(t) + R_{dc} \cdot i_{dc}(t)$$

$$di_{sdq}(t) = -W \cdot i_{sdq}(t) + \frac{-R_s}{L_s} \cdot i_{sdq}(t) - \frac{1}{L_s} \cdot v_{rdq_n}(t) + \frac{1}{L_s} \cdot v_{sdq}(t)$$

$$dv_{rdq_n}(t) = -W \cdot v_{rdq_n}(t) + \frac{-1}{C_r} \cdot m_{rdq}(t) \cdot i_{dc}(t) + \frac{1}{C_r} \cdot i_{sdq}(t)$$

$$di_{dc}(t) = \frac{-R_{dc}}{L_{dc}} \cdot i_{dc}(t) + \frac{1}{L_{dc}} \cdot v_{rdq_n}(t)^T \cdot m_{rdq}(t)$$

$$v_{sdq}(t) := (\sqrt{3} \cdot 220 \ 0)^T$$



Parámetros

$$L_s := 30 \cdot 10^{-3}$$

$$R_s := 1$$

$$C_r := 50 \cdot 10^{-6}$$

$$R_{dc} := 10$$

$$L_{dc} := 30 \cdot 10^{-3}$$

$$W := \begin{pmatrix} 0 & -\omega_s \\ \omega_s & 0 \end{pmatrix}$$

$$m_{rdq}(t) := \sqrt{\frac{2}{3}} \cdot \begin{pmatrix} \sin(\omega_s \cdot t) & \sin(\omega_s \cdot t - 2 \cdot \frac{\pi}{3}) & \sin(\omega_s \cdot t - 4 \cdot \frac{\pi}{3}) \\ \cos(\omega_s \cdot t) & \cos(\omega_s \cdot t - 2 \cdot \frac{\pi}{3}) & \cos(\omega_s \cdot t - 4 \cdot \frac{\pi}{3}) \end{pmatrix} \cdot m_r(t)$$

Simulación $t_f := 0.02$ $n_f := 2048$ $n := 1 \dots n_f$ $t := 0, \frac{t_f}{n_f} \dots t_f$

$$D(t, x) := \text{stack} \left(-W \cdot (x_1 \ x_2)^T + \frac{-R_s}{L_s} \cdot (x_1 \ x_2)^T - \frac{1}{L_s} \cdot (x_3 \ x_4)^T + \frac{1}{L_s} \cdot v_{sdq}(t), -W \cdot (x_3 \ x_4)^T + \frac{-1}{C_r} \cdot m_{rdq}(t) \cdot x_5 + \frac{1}{C_r} \cdot (x_1 \ x_2)^T, \frac{-R_{dc}}{L_{dc}} \cdot x_5 + \frac{1}{L_{dc}} \cdot (x_3 \ x_4)^T \cdot m_{rdq}(t) \right)$$

$$CI := (51.206 \ 6.078 \ 386.785 \ -488.94 \ 41.089)^T$$

$$Z := \text{rkfixed}(CI, 0, t_f, n_f, D)$$

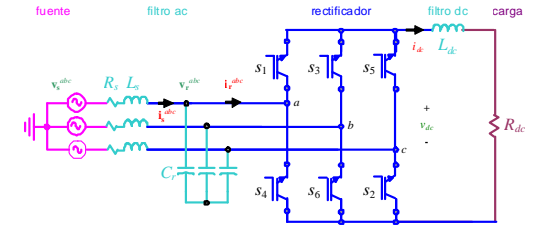
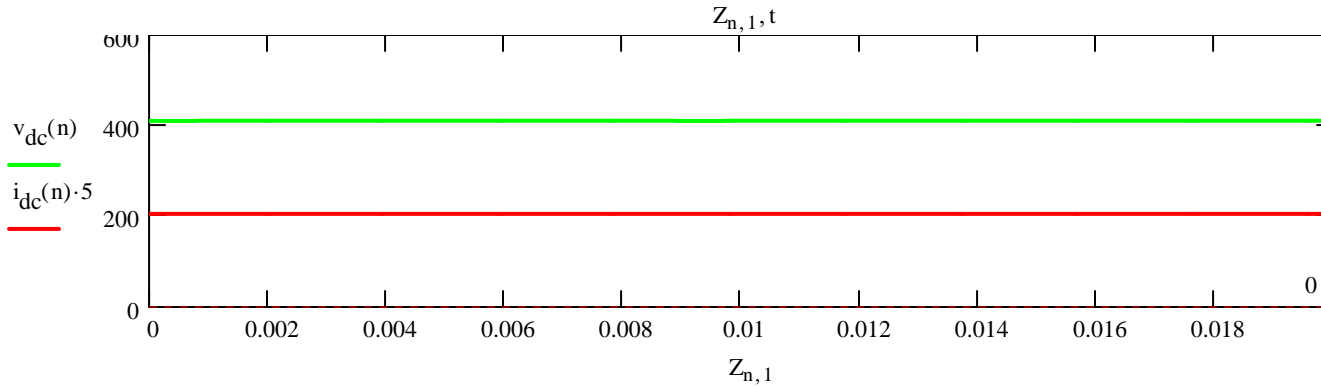
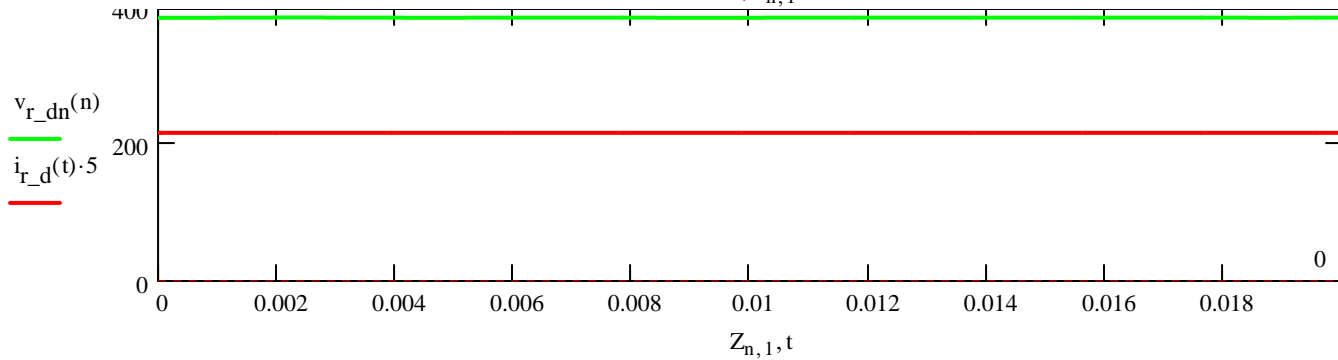
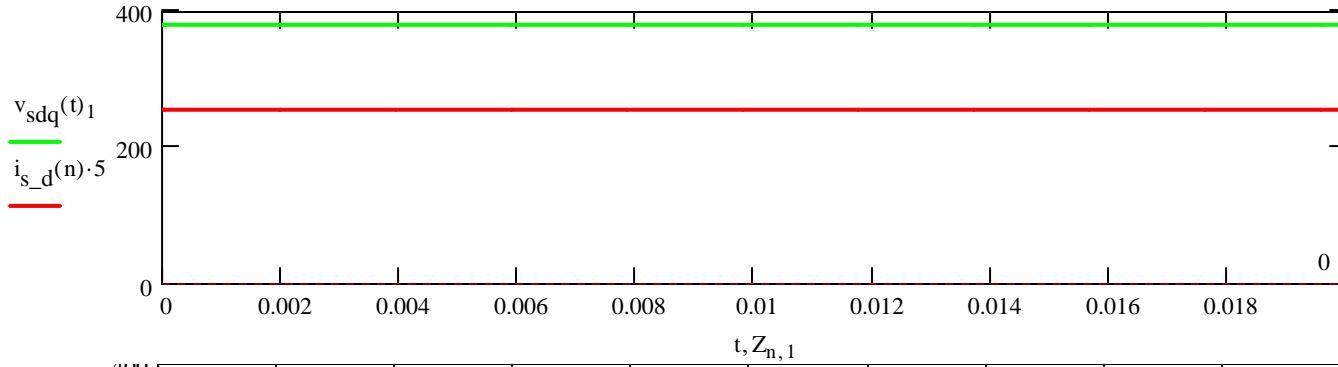
$$CI := (Z_{n_f, 2} \ Z_{n_f, 3} \ Z_{n_f, 4} \ Z_{n_f, 5} \ Z_{n_f, 6})^T$$

$$Z := \text{rkfixed}(CI, 0, t_f, n_f, D)$$

$$i_{dc}(n) := Z_{n,6} \quad i_{r_d}(t) := \left(m_{rdq}(t) \cdot i_{dc} \left(t \cdot \frac{n_f}{t_f} \right) \right)_1 \quad i_{r_q}(t) := \left(m_{rdq}(t) \cdot i_{dc} \left(t \cdot \frac{n_f}{t_f} \right) \right)_2$$

$$i_{s_d}(n) := Z_{n,2} \quad i_{s_q}(n) := Z_{n,3} \quad v_{r_dn}(n) := Z_{n,4} \quad v_{r_qn}(n) := Z_{n,5}$$

$$v_{dc}(n) := m_{rdq} \left(n \cdot \frac{t_f}{n_f} \right)^T \cdot (v_{r_dn}(n) \quad v_{r_qn}(n))^T$$



$$\sqrt{i_{r_d}(0.01)^2 + i_{r_q}(0.01)^2} \cdot \frac{\sqrt{2}}{3} = 35.557$$

$$\frac{\sqrt{2}}{3} \cdot |m_{rdq}(0.01)| \cdot i_{dc}(1) = 35.557$$

$$\frac{\sqrt{3}}{2} \cdot M \cdot i_{dc}(1) = 35.557$$

La fundamental de i_r es $0.866 M I_{dc}$

Punto de operación del Rectificador de Corriente Trifásico en dq0

Problema Encontrar un punto de operación

$$\phi_0 := -30 \cdot \frac{\pi}{180}$$

$$P_{dc_0} := 4000$$

$$\begin{pmatrix} V_{sd} \\ V_{sq} \end{pmatrix} := \begin{pmatrix} \sqrt{3} \cdot 220 \\ 0 \end{pmatrix}$$

c.i. para Given/Find que deben ser igual en número al número de incógnitas

$$\begin{pmatrix} I_{sd} \\ I_{sq} \end{pmatrix} := \begin{pmatrix} 10 \\ -6 \end{pmatrix}$$

$$\begin{pmatrix} V_{rd} \\ V_{rq} \end{pmatrix} := \begin{pmatrix} 300 \\ 0 \end{pmatrix}$$

$$\begin{pmatrix} M_{rd} \\ M_{rq} \end{pmatrix} := \begin{pmatrix} 0.5 \\ 0.0 \end{pmatrix}$$

$$I_{dc} := 20$$

Given

$$\begin{pmatrix} 0 \\ 0 \end{pmatrix} = -W \cdot \begin{pmatrix} I_{sd} \\ I_{sq} \end{pmatrix} + \frac{-R_s}{L_s} \cdot \begin{pmatrix} I_{sd} \\ I_{sq} \end{pmatrix} - \frac{1}{L_s} \cdot \begin{pmatrix} V_{rd} \\ V_{rq} \end{pmatrix} + \frac{1}{L_s} \cdot \begin{pmatrix} V_{sd} \\ V_{sq} \end{pmatrix}$$

$$0 = \frac{-R_{dc}}{L_{dc}} \cdot I_{dc} + \frac{1}{L_{dc}} \cdot \begin{pmatrix} V_{rd} \\ V_{rq} \end{pmatrix}^T \cdot \begin{pmatrix} M_{rd} \\ M_{rq} \end{pmatrix}$$

$$\begin{pmatrix} 0 \\ 0 \end{pmatrix} = -W \cdot \begin{pmatrix} V_{rd} \\ V_{rq} \end{pmatrix} + \frac{-1}{C_r} \cdot \begin{pmatrix} M_{rd} \\ M_{rq} \end{pmatrix} \cdot I_{dc} + \frac{1}{C_r} \cdot \begin{pmatrix} I_{sd} \\ I_{sq} \end{pmatrix}$$

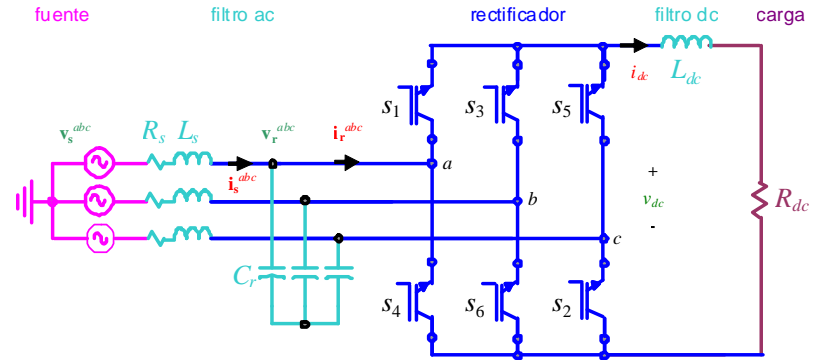
$$\phi_0 = \text{atan} \left(\frac{I_{sq}}{I_{sd}} \right)$$

$$P_{dc_0} = R_{dc} \cdot I_{dc}^2$$

$$\begin{pmatrix} I_{sd} & I_{sq} & V_{rd} & V_{rq} & I_{dc} & M_{rd} & M_{rq} \end{pmatrix} := \text{Find}(I_{sd}, I_{sq}, V_{rd}, V_{rq}, I_{dc}, M_{rd}, M_{rq})^T$$

$$m_{rdq}(t) := \begin{pmatrix} M_{rd} & M_{rq} \end{pmatrix}^T$$

$$\begin{pmatrix} I_{sd} & I_{sq} & V_{rd} & V_{rq} & I_{dc} & M_{rd} & M_{rq} \end{pmatrix} = (10.914 \quad -6.301 \quad 310.749 \quad -96.562 \quad 20 \quad 0.47 \quad -0.559)$$



Ángulo de Corriente

$$\phi := \text{atan} \left(\frac{I_{sq}}{I_{sd}} \right)$$

$$\phi \cdot \frac{180}{\pi} = -30$$

Potencia en la Carga

$$P_{dc_0} := R_{dc} \cdot I_{dc}^2$$

$$P_{dc_0} \cdot 10^{-3} = 4$$

Ampl. Mod. en abc

$$M_r := \frac{2}{\sqrt{3}} \cdot \sqrt{\frac{2}{3} \cdot \sqrt{(M_{rd})^2 + (M_{rq})^2}}$$

$$M_r = 0.689$$

Filtro AC

$$L_s \cdot 10^3 = 30$$

$$C_r \cdot 10^6 = 50$$

Frec. de Resonancia:

$$\omega_{rn} := (\omega_s \cdot \sqrt{L_s \cdot C_r})^{-1}$$

$$\omega_{rn} = 2.599$$

¿ Especificar un índice de modulación M_r ?

Punto de operación del Rectificador de Corriente Trifásico en dq0

Problema Encontrar un punto de operación

$$\phi_0 \cdot \frac{180}{\pi} = -30$$

$$P_{dc_0} = 4 \times 10^3$$

$$M_r := 0.8$$

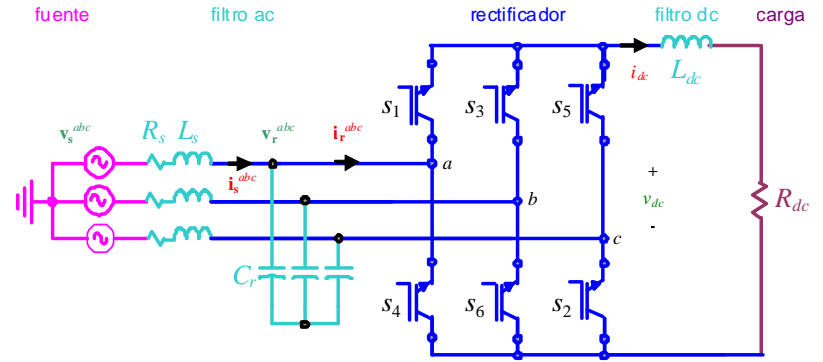
c.i. para Given/Find que deben ser igual en número al número de incógnitas

$$\begin{pmatrix} I_{sd} \\ I_{sq} \end{pmatrix} = \begin{pmatrix} 10.914 \\ -6.301 \end{pmatrix}$$

$$\begin{pmatrix} V_{rd} \\ V_{rq} \end{pmatrix} = \begin{pmatrix} 310.749 \\ -96.562 \end{pmatrix}$$

$$\begin{pmatrix} M_{rd} \\ M_{rq} \end{pmatrix} = \begin{pmatrix} 0.47 \\ -0.559 \end{pmatrix}$$

$$I_{dc} := 20$$



Given

$$\begin{pmatrix} 0 \\ 0 \end{pmatrix} = -W \cdot \begin{pmatrix} I_{sd} \\ I_{sq} \end{pmatrix} + \frac{-R_s}{L_s} \cdot \begin{pmatrix} I_{sd} \\ I_{sq} \end{pmatrix} - \frac{1}{L_s} \cdot \begin{pmatrix} V_{rd} \\ V_{rq} \end{pmatrix} + \frac{1}{L_s} \cdot \begin{pmatrix} V_{sd} \\ V_{sq} \end{pmatrix}$$

$$0 = \frac{-R_{dc}}{L_{dc}} \cdot I_{dc} + \frac{1}{L_{dc}} \cdot \begin{pmatrix} V_{rd} \\ V_{rq} \end{pmatrix}^T \cdot \begin{pmatrix} M_{rd} \\ M_{rq} \end{pmatrix}$$

$$M_r = \frac{2}{\sqrt{3}} \cdot \frac{\sqrt{2}}{\sqrt{3}} \cdot \sqrt{(M_{rd})^2 + (M_{rq})^2}$$

$$\begin{pmatrix} 0 \\ 0 \end{pmatrix} = -W \cdot \begin{pmatrix} V_{rd} \\ V_{rq} \end{pmatrix} + \frac{-1}{C_r} \cdot \begin{pmatrix} M_{rd} \\ M_{rq} \end{pmatrix} \cdot I_{dc} + \frac{1}{C_r} \cdot \begin{pmatrix} I_{sd} \\ I_{sq} \end{pmatrix}$$

$$\phi_0 = \text{atan} \left(\frac{I_{sq}}{I_{sd}} \right)$$

$$P_{dc_0} = R_{dc} \cdot I_{dc}^2$$

$$(I_{sd} \ I_{sq} \ V_{rd} \ V_{rq} \ I_{dc} \ M_{rd} \ M_{rq} \ C_r) := \text{Find}(I_{sd}, I_{sq}, V_{rd}, V_{rq}, I_{dc}, M_{rd}, M_{rq}, C_r)^T$$

Se encuentra el Capacitor AC apropiado

$$m_{rdq}(t) := (M_{rd} \ M_{rq})^T$$

$$(I_{sd} \ I_{sq} \ V_{rd} \ V_{rq} \ I_{dc} \ M_{rd} \ M_{rq} \ C_r) = (10.914 \ -6.301 \ 310.749 \ -96.562 \ 20 \ 0.413 \ -0.741 \ 8.727 \times 10^{-5})$$

Ángulo de Corriente

Potencia en la Carga

Ampl. Mod. en abc

Filtro AC

Frec. de Resonancia:

$$\phi := \text{atan} \left(\frac{I_{sq}}{I_{sd}} \right)$$

$$P_{dc_0} := R_{dc} \cdot I_{dc}^2$$

$$M_r := \frac{2}{\sqrt{3}} \cdot \frac{\sqrt{2}}{\sqrt{3}} \cdot \sqrt{(M_{rd})^2 + (M_{rq})^2}$$

$$L_s \cdot 10^3 = 30$$

$$\omega_{rn} := (\omega_s \cdot \sqrt{L_s \cdot C_r})^{-1}$$

$$\phi \cdot \frac{180}{\pi} = -30$$

$$P_{dc_0} \cdot 10^{-3} = 4$$

$$M_r = 0.8$$

$$C_r \cdot 10^6 = 87.273$$

$$\omega_{rn} = 1.967$$

¿ Epecificar una frec. de resonancia ?

Punto de operación del Rectificador de Corriente Trifásico en dq0

Problema Encontrar un punto de operación

$$\phi_0 \cdot \frac{180}{\pi} = -30$$

$$P_{dc_0} = 4 \times 10^3$$

$$M_r = 0.8$$

$$\omega_{rn} := 3$$

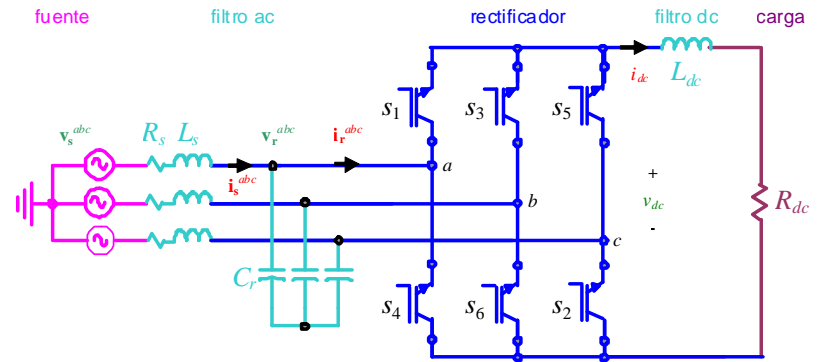
c.i. para Given/Find que deben ser igual en número al número de incógnitas

$$\begin{pmatrix} I_{sd} \\ I_{sq} \end{pmatrix} = \begin{pmatrix} 10.914 \\ -6.301 \end{pmatrix}$$

$$\begin{pmatrix} V_{rd} \\ V_{rq} \end{pmatrix} = \begin{pmatrix} 310.749 \\ -96.562 \end{pmatrix}$$

$$\begin{pmatrix} M_{rd} \\ M_{rq} \end{pmatrix} = \begin{pmatrix} 0.413 \\ -0.741 \end{pmatrix}$$

$$I_{dc} = 20$$



Given

$$\begin{pmatrix} 0 \\ 0 \end{pmatrix} = -W \cdot \begin{pmatrix} I_{sd} \\ I_{sq} \end{pmatrix} + \frac{-R_s}{L_s} \cdot \begin{pmatrix} I_{sd} \\ I_{sq} \end{pmatrix} - \frac{1}{L_s} \cdot \begin{pmatrix} V_{rd} \\ V_{rq} \end{pmatrix} + \frac{1}{L_s} \cdot \begin{pmatrix} V_{sd} \\ V_{sq} \end{pmatrix}$$

$$0 = \frac{-R_{dc}}{L_{dc}} \cdot I_{dc} + \frac{1}{L_{dc}} \cdot \begin{pmatrix} V_{rd} \\ V_{rq} \end{pmatrix}^T \cdot \begin{pmatrix} M_{rd} \\ M_{rq} \end{pmatrix}$$

$$M_r = \frac{2}{\sqrt{3}} \cdot \sqrt{\frac{2}{3}} \cdot \sqrt{(M_{rd})^2 + (M_{rq})^2}$$

$$\begin{pmatrix} 0 \\ 0 \end{pmatrix} = -W \cdot \begin{pmatrix} V_{rd} \\ V_{rq} \end{pmatrix} + \frac{-1}{C_r} \cdot \begin{pmatrix} M_{rd} \\ M_{rq} \end{pmatrix} \cdot I_{dc} + \frac{1}{C_r} \cdot \begin{pmatrix} I_{sd} \\ I_{sq} \end{pmatrix}$$

$$\phi_0 = \text{atan} \left(\frac{I_{sq}}{I_{sd}} \right)$$

$$P_{dc_0} = R_{dc} \cdot I_{dc}^2$$

$$\omega_{rn} = (\omega_s \cdot \sqrt{L_s \cdot C_r})^{-1}$$

$$\begin{pmatrix} I_{sd} & I_{sq} & V_{rd} & V_{rq} & I_{dc} & M_{rd} & M_{rq} & C_r & L_s \end{pmatrix} := \text{Find}(I_{sd}, I_{sq}, V_{rd}, V_{rq}, I_{dc}, M_{rd}, M_{rq}, C_r, L_s)^T$$

Se encuentra el Inductor AC apropiado

$$m_{rdq}(t) := \begin{pmatrix} M_{rd} & M_{rq} \end{pmatrix}^T$$

$$\begin{pmatrix} I_{sd} & I_{sq} & V_{rd} & V_{rq} & I_{dc} & M_{rd} & M_{rq} & C_r & L_s \end{pmatrix} = \begin{pmatrix} 10.914 & -6.301 & 338.629 & -48.273 & 20 & 0.492 & -0.691 & 7.073 \times 10^{-5} & 0.016 \end{pmatrix}$$

Ángulo de Corriente

Potencia en la Carga

Ampl. Mod. en abc

Filtro AC

Frec. de Resonancia:

$$\phi := \text{atan} \left(\frac{I_{sq}}{I_{sd}} \right)$$

$$P_{dc_0} := R_{dc} \cdot I_{dc}^2$$

$$M_r := \frac{2}{\sqrt{3}} \cdot \sqrt{\frac{2}{3}} \cdot \sqrt{(M_{rd})^2 + (M_{rq})^2}$$

$$L_s \cdot 10^3 = 15.917$$

$$\omega_{rn} := (\omega_s \cdot \sqrt{L_s \cdot C_r})^{-1}$$

$$\phi \cdot \frac{180}{\pi} = -30$$

$$P_{dc_0} \cdot 10^{-3} = 4$$

$$M_r = 0.8$$

$$C_r \cdot 10^6 = 70.73$$

$$\omega_{rn} = 3$$

Punto de operación del Rectificador de Corriente Trifásico en abc

Problema Estudiar el modelo del rectificador de corriente con Modulación SPWM.

La moduladora es,

$$m_r(t) := T_{abc_dq0}(t)^T \cdot \begin{pmatrix} M_{rd} \\ M_{rq} \\ 0 \end{pmatrix}$$

$$m_a(t) := \frac{2}{\sqrt{3}} \cdot m_r(t)_1$$

$$m_b(t) := \frac{2}{\sqrt{3}} \cdot m_r(t)_2$$

$$m_c(t) := \frac{2}{\sqrt{3}} \cdot m_r(t)_3$$

$$M := \sqrt{\frac{2}{3} \cdot \sqrt{m_a(0)^2 + m_b(0)^2 + m_c(0)^2}}$$

$$f_M := \text{atan}\left(\frac{M_{rq}}{M_{rd}}\right)$$

$$M = 0.8$$

$$f_M \cdot \frac{180}{\pi} = -54.556$$

La triangular es,

$$f_{n_tr} := 15 \text{ per} := 1$$

$$\text{tri}(t) := \frac{2}{\pi} \cdot \text{asin}\left(\sin\left(f_{n_tr} \cdot \omega_s \cdot t + f_M \cdot f_{n_tr} - \frac{\pi}{2}\right)\right)$$

$$m_{ax}(t) := (m_a(t) - m_b(t)) \cdot (\sqrt{3})^{-1}$$

$$s_x(t) := \text{if}(m_{ax}(t) > \text{tri}(t), 1, 0)$$

$$m_{bx}(t) := (m_b(t) - m_c(t)) \cdot (\sqrt{3})^{-1}$$

$$s_y(t) := \text{if}(m_{bx}(t) > \text{tri}(t), 1, 0)$$

$$m_{cx}(t) := (m_c(t) - m_a(t)) \cdot (\sqrt{3})^{-1}$$

$$s_z(t) := \text{if}(m_{cx}(t) > \text{tri}(t), 1, 0)$$

$$s_1(t) := s_x(t) \cdot s_{zn}(t)$$

$$s_4(t) := s_z(t) \cdot s_{xn}(t)$$

$$s_3(t) := s_y(t) \cdot s_{xn}(t)$$

$$s_6(t) := s_x(t) \cdot s_{yn}(t)$$

$$s_5(t) := s_z(t) \cdot s_{yn}(t)$$

$$s_2(t) := s_y(t) \cdot s_{zn}(t)$$

$$R_s = 1$$

$$C_r \cdot 10^6 = 70.73$$

$$L_s \cdot 10^3 = 15.917$$

$$L_{dc} \cdot 10^3 = 30$$

$$R_{dc} = 10$$

$$s_{xn}(t) := \text{if}(s_x(t) = 1, 0, 1)$$

$$s_{yn}(t) := \text{if}(s_y(t) = 1, 0, 1)$$

$$s_{zn}(t) := \text{if}(s_z(t) = 1, 0, 1)$$

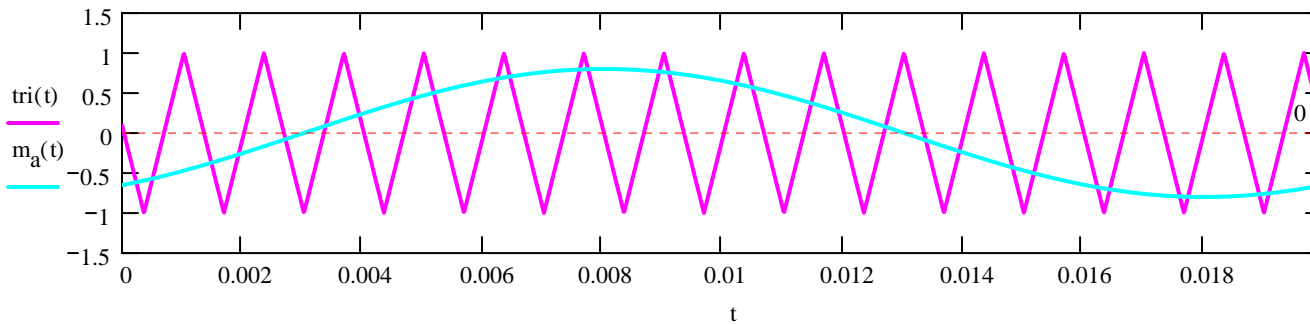
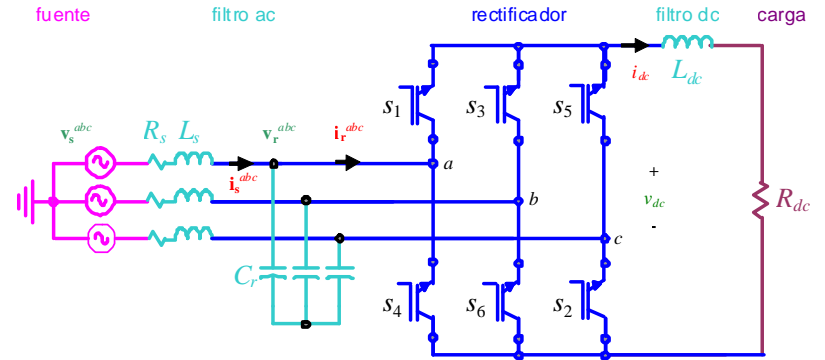
$$s_a(t) := s_1(t) - s_4(t)$$

$$s_b(t) := s_3(t) - s_6(t)$$

$$s_c(t) := s_5(t) - s_2(t)$$

$$s_r(t) := \begin{pmatrix} s_a(t) \\ s_b(t) \\ s_c(t) \end{pmatrix}$$

$$v_s(t) := T_{abc_dq0}(t)^T \cdot \begin{pmatrix} V_{sd} \\ V_{sq} \\ 0 \end{pmatrix}$$



Simulación $t_f := 0.02$ $n_f := 2048$ $n := 1 .. n_f$ $t := 0, \frac{t_f}{n_f} .. t_f$

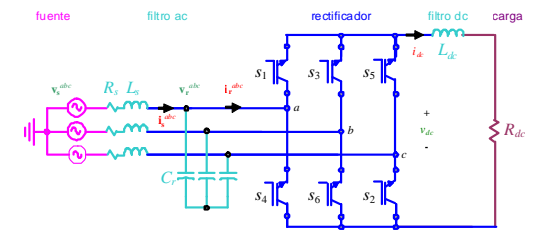
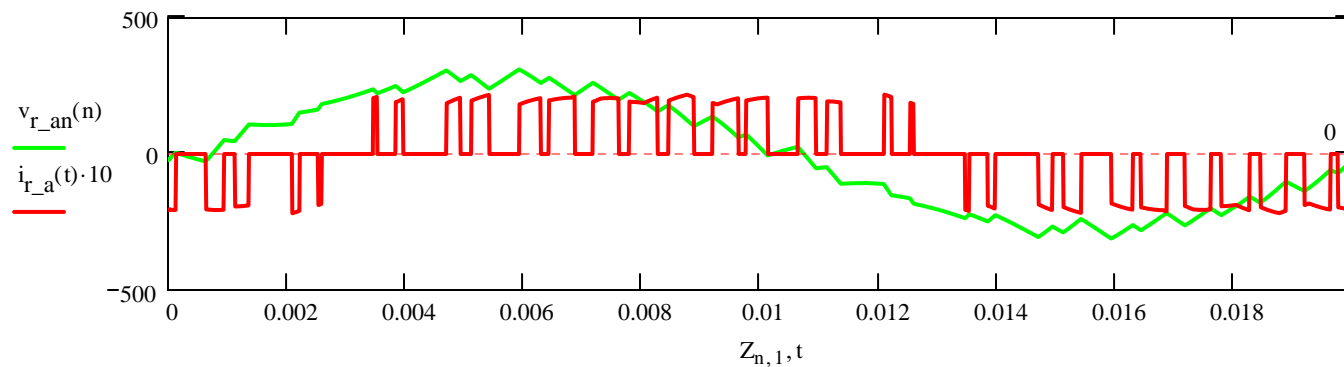
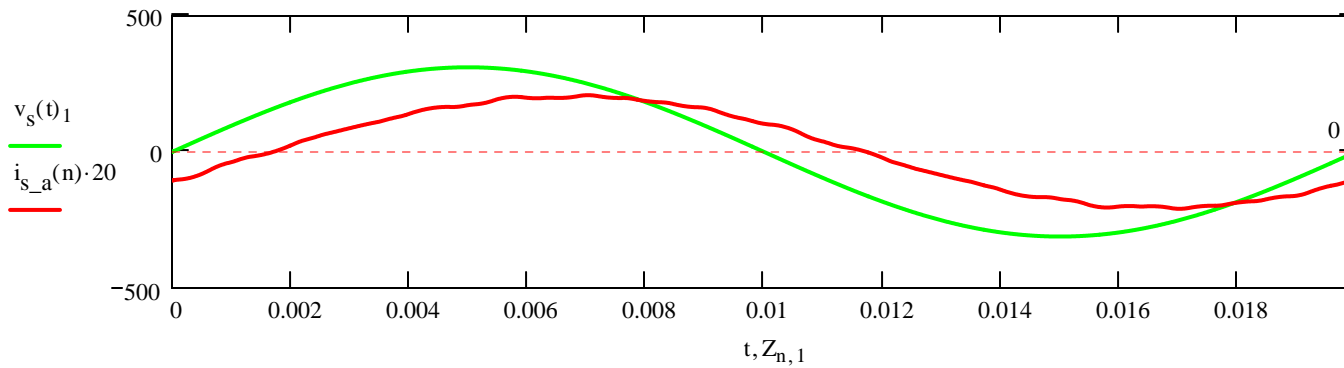
$$D(t, x) := \text{stack} \left(\frac{-R_s}{L_s} \cdot (x_1 \ x_2 \ x_3)^T - \frac{1}{L_s} \cdot (x_4 \ x_5 \ x_6)^T + \frac{1}{L_s} \cdot v_s(t), \frac{-1}{C_r} \cdot s_r(t) \cdot x_7 + \frac{1}{C_r} \cdot (x_1 \ x_2 \ x_3)^T, \frac{-R_{dc}}{L_{dc}} \cdot x_7 + \frac{1}{L_{dc}} \cdot (x_4 \ x_5 \ x_6)^T \cdot s_r(t) \right)$$

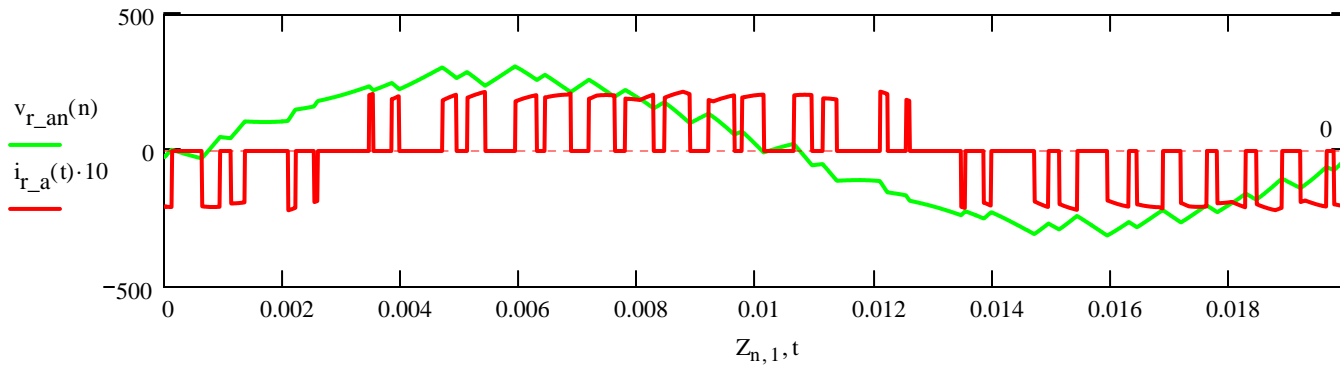
$$CI := (-5.208 \ -4.926 \ 10.134 \ -20.061 \ -230.723 \ 250.783 \ 20.47)^T \quad Z := \text{rkfixed}(CI, 0, t_f, n_f, D)$$

$$CI := (Z_{n_f,2} \ Z_{n_f,3} \ Z_{n_f,4} \ Z_{n_f,5} \ Z_{n_f,6} \ Z_{n_f,7} \ Z_{n_f,8})^T \quad Z := \text{rkfixed}(CI, 0, t_f, n_f, D) \quad i_{s_a}(n) := Z_{n,2} \quad i_{s_b}(n) := Z_{n,3} \quad i_{s_c}(n) := Z_{n,4}$$

$$i_{dc}(n) := Z_{n,8} \quad i_{r_a}(t) := \left(s_r(t) \cdot i_{dc} \left(t \cdot \frac{n_f}{t_f} \right) \right)_1 \quad i_{r_b}(t) := \left(s_r(t) \cdot i_{dc} \left(t \cdot \frac{n_f}{t_f} \right) \right)_2 \quad i_{r_c}(t) := \left(s_r(t) \cdot i_{dc} \left(t \cdot \frac{n_f}{t_f} \right) \right)_3 \quad v_{r_an}(n) := Z_{n,5} \quad v_{r_bn}(n) := Z_{n,6} \quad v_{r_cn}(n) := Z_{n,7}$$

$$v_{dc}(n) := s_r \left(n \cdot \frac{t_f}{n_f} \right)^T \cdot (v_{r_an}(n) \ v_{r_bn}(n) \ v_{r_cn}(n))^T$$

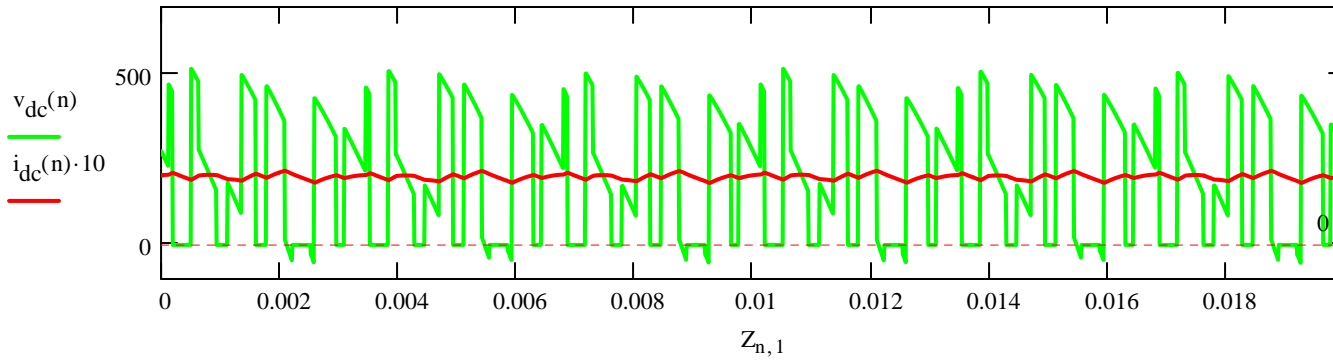
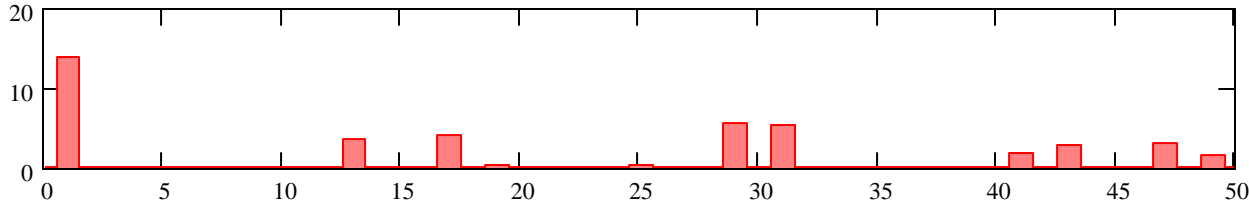




```

N := 1024          m := 1..N
x_m := i_r_a((m/N)*t_f)  xf := FFT(x)
xv(m) := if(m = 1, 1, 2) * xf_m_per
| xv(2) | = 13.886
    
```

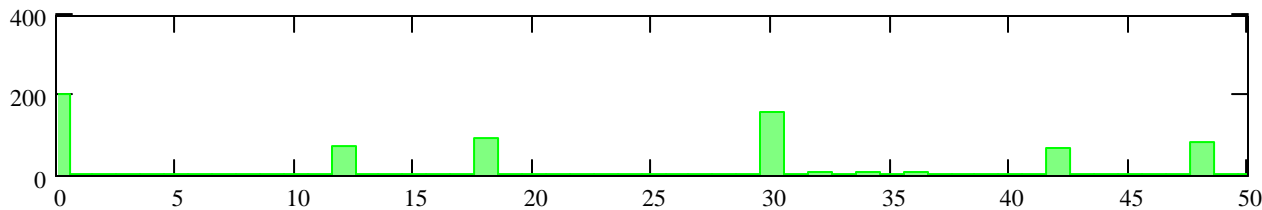
FFT de i_{r_a}



```

N := 1024          m := 1..N
x_m := v_dc((m/N)*n_f)  xf := FFT(x)
xv(m) := if(m = 1, 1, 2) * xf_m_per
| xv(1) | = 203.235  V_dc := | xv(1) |
P_o := (V_dc^2) / R_dc    P_o = 4.13 * 10^3
    
```

FFT de v_{dc}



El voltaje DC no tiene segunda armónica. Sólo armónicas de conmutación.

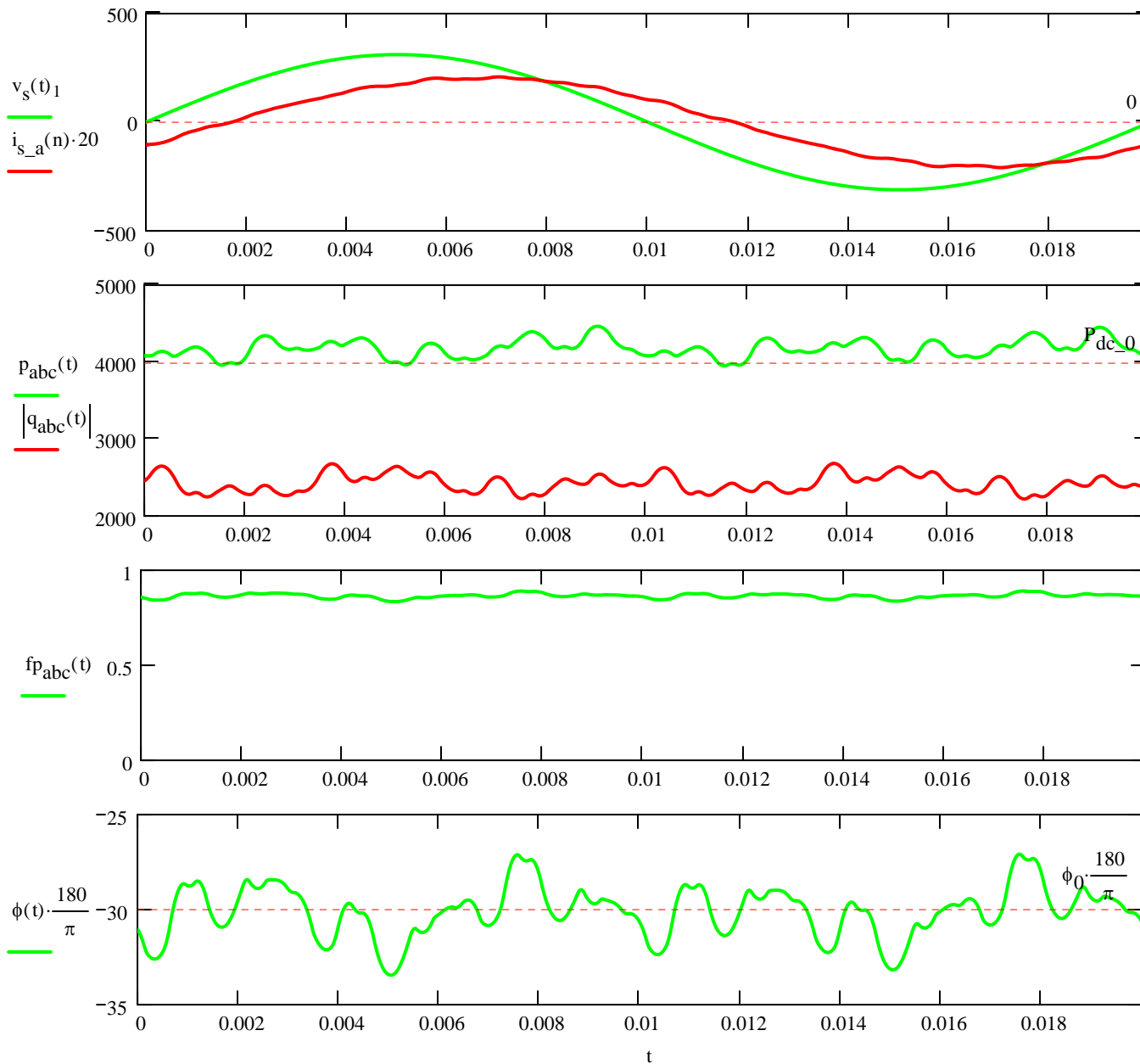
$$v_{abc}(t) := v_s(t) \quad i_{abc}(t) := \left(i_{s_a} \left(t \cdot \frac{n_f}{t_f} \right) \quad i_{s_b} \left(t \cdot \frac{n_f}{t_f} \right) \quad i_{s_c} \left(t \cdot \frac{n_f}{t_f} \right) \right)^T \quad P_{abc}(t) := v_{abc}(t)^T \cdot i_{abc}(t)$$

$$q_{abc}(t) := v_{abc}(t) \times i_{abc}(t)$$

$$s_{abc}(t) := \sqrt{(|v_{abc}(t)|)^2 \cdot (|i_{abc}(t)|)^2}$$

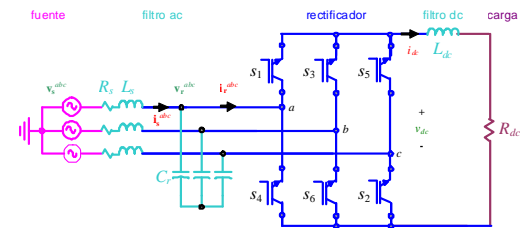
$$f_{p_{abc}}(t) := \frac{P_{abc}(t)}{s_{abc}(t)}$$

$$\phi(t) := \text{atan} \left[\frac{(T_{abc_dq0}(t) \cdot i_{abc}(t))_2}{(T_{abc_dq0}(t) \cdot i_{abc}(t))_1} \right]$$



El sistema si está en S.S.

¿ Qué rangos puede alcanzar el sistema?... **La Región de Operación** entrega esta respuesta.



Región de Operación del RFC Trifásico en dq0

Problema Estudiar el modelo promedio en dq0 del rectificador de voltaje. $t := 0$

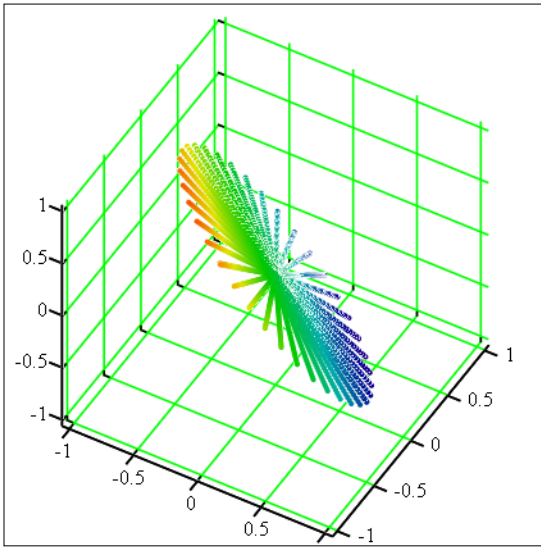
$$m_{r_abc}(M, f_M) := \frac{\sqrt{3}}{2} \cdot \begin{pmatrix} M \cdot \sin\left(\omega_s \cdot t + f_M - \frac{0 \cdot \pi}{3}\right) \\ M \cdot \sin\left(\omega_s \cdot t + f_M - \frac{2 \cdot \pi}{3}\right) \\ M \cdot \sin\left(\omega_s \cdot t + f_M - \frac{4 \cdot \pi}{3}\right) \end{pmatrix}$$

$$X_a(M, f_M) := m_{r_abc}(M, f_M)_1$$

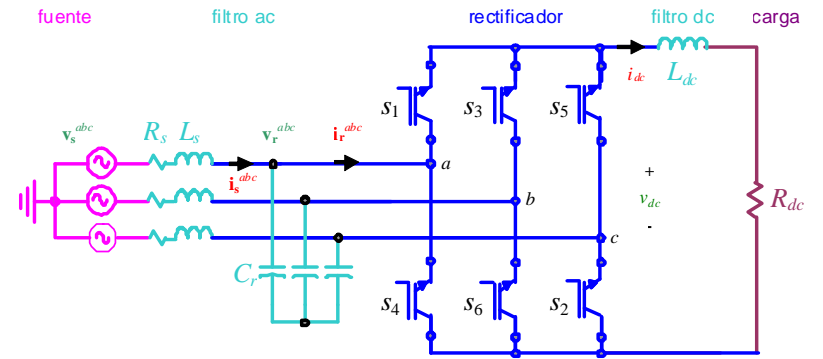
$$Y_b(M, f_M) := m_{r_abc}(M, f_M)_2$$

$$Z_c(M, f_M) := m_{r_abc}(M, f_M)_3$$

Las señales en abc en función de M y f_M .



(X_a, Y_b, Z_c)



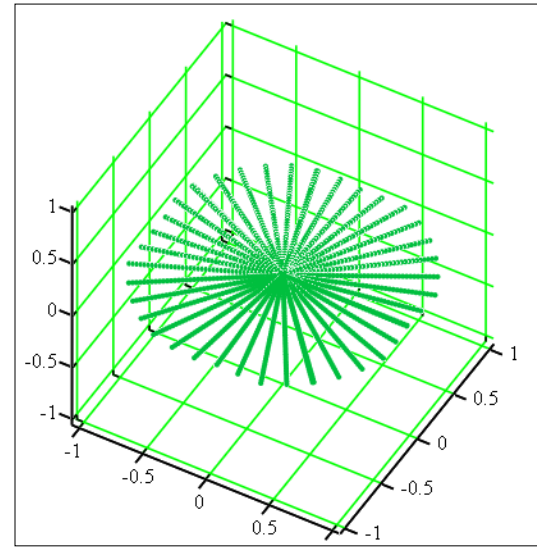
$$m_{r_dq0}(M, f_M) := T_{abc_dq0}(t) \cdot m_{r_abc}(M, f_M)$$

$$X_d(M, f_M) := m_{r_dq0}(M, f_M)_1$$

$$Y_q(M, f_M) := m_{r_dq0}(M, f_M)_2$$

$$Z_0(M, f_M) := m_{r_dq0}(M, f_M)_3$$

Las señales en dq0 en función de M y f_M .



(X_d, Y_q, Z_0)

c.i. para Given/Find que deben ser igual en número al número de incógnitas

$$\begin{pmatrix} I_{sd} \\ I_{sq} \end{pmatrix} := \begin{pmatrix} 10 \\ -10 \end{pmatrix}$$

$$\begin{pmatrix} V_{rd} \\ V_{rq} \end{pmatrix} := \begin{pmatrix} 100 \\ 0 \end{pmatrix}$$

$$\begin{pmatrix} M_{rd} \\ M_{rq} \end{pmatrix} := \begin{pmatrix} 0.5 \\ 0 \end{pmatrix}$$

$$I_{dc} := 20$$

$$\begin{pmatrix} V_{sd} \\ V_{sq} \end{pmatrix} := \begin{pmatrix} \sqrt{3} \cdot 220 \\ 0 \end{pmatrix}$$

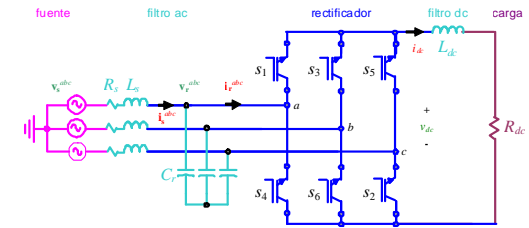
$$\text{Max} := \frac{\sqrt{3}}{2} \cdot \sqrt{\frac{3}{2}}$$

Given

$$\begin{pmatrix} 0 \\ 0 \end{pmatrix} = -W \cdot \begin{pmatrix} I_{sd} \\ I_{sq} \end{pmatrix} + \frac{-R_s}{L_s} \cdot \begin{pmatrix} I_{sd} \\ I_{sq} \end{pmatrix} - \frac{1}{L_s} \cdot \begin{pmatrix} V_{rd} \\ V_{rq} \end{pmatrix} + \frac{1}{L_s} \cdot \begin{pmatrix} V_{sd} \\ V_{sq} \end{pmatrix}$$

$$0 = \frac{-R_{dc}}{L_{dc}} \cdot I_{dc} + \frac{1}{L_{dc}} \cdot \begin{pmatrix} V_{rd} \\ V_{rq} \end{pmatrix}^T \cdot \begin{pmatrix} M_{rd} \\ M_{rq} \end{pmatrix}$$

$$\begin{pmatrix} 0 \\ 0 \end{pmatrix} = -W \cdot \begin{pmatrix} V_{rd} \\ V_{rq} \end{pmatrix} + \frac{-1}{C_r} \cdot \begin{pmatrix} M_{rd} \\ M_{rq} \end{pmatrix} \cdot I_{dc} + \frac{1}{C_r} \cdot \begin{pmatrix} I_{sd} \\ I_{sq} \end{pmatrix}$$



$$\text{Sol}(M_{rd}, M_{rq}) := \text{Find}(I_{sd}, I_{sq}, V_{rd}, V_{rq}, I_{dc})$$

Se graficará para M_{rd} y M_{rq} en el rango $-\text{Max}$ a Max .

$$\text{me} := 40 \quad \text{mi}_1 := -\text{Max} \quad \text{ma}_1 := \text{Max} \quad \text{mi}_2 := -\text{Max} \quad \text{ma}_2 := \text{Max}$$

A graficar I_{sd} , I_{sq} y I_{dc}

$$I_{sd}(x_d, x_q) := \text{Sol}(x_d, x_q)_1$$

$$I_{sq}(x_d, x_q) := \text{Sol}(x_d, x_q)_2$$

$$I_{dc}(x_d, x_q) := \text{Sol}(x_d, x_q)_5$$

$$S_{I_{sd}} := \text{CreateMesh}(I_{sd}, \text{mi}_2, \text{ma}_2, \text{mi}_1, \text{ma}_1, \text{me})$$

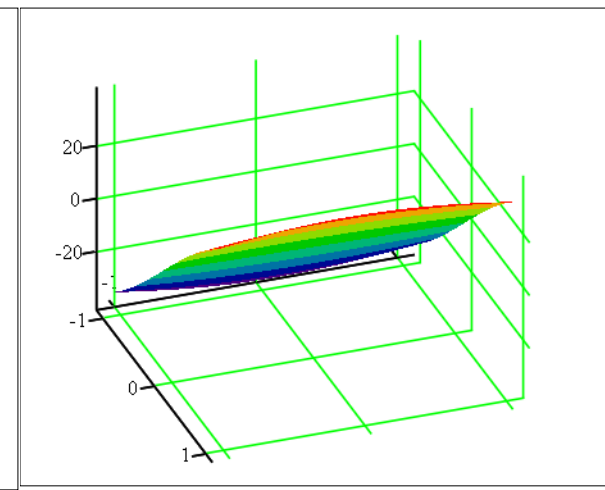
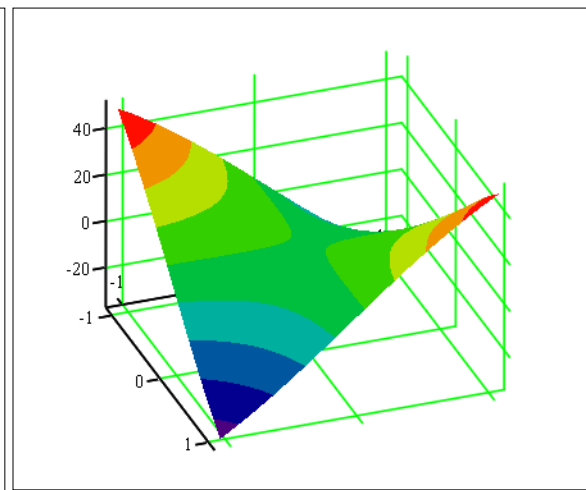
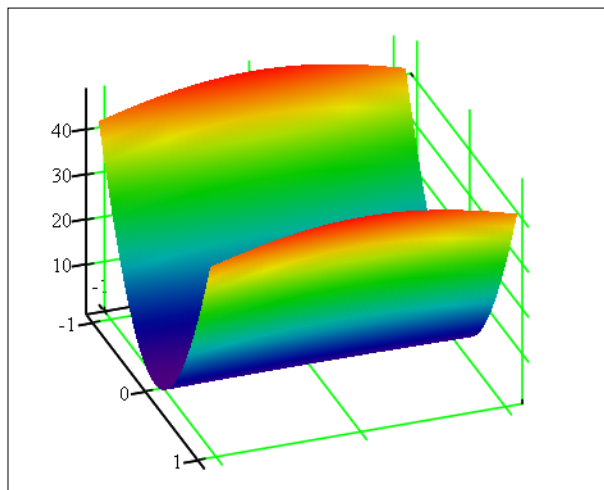
$$S_{I_{sq}} := \text{CreateMesh}(I_{sq}, \text{mi}_2, \text{ma}_2, \text{mi}_1, \text{ma}_1, \text{me})$$

$$S_{I_{dc}} := \text{CreateMesh}(I_{dc}, \text{mi}_2, \text{ma}_2, \text{mi}_1, \text{ma}_1, \text{me})$$

Corriente I_{sd}

Corriente I_{sq}

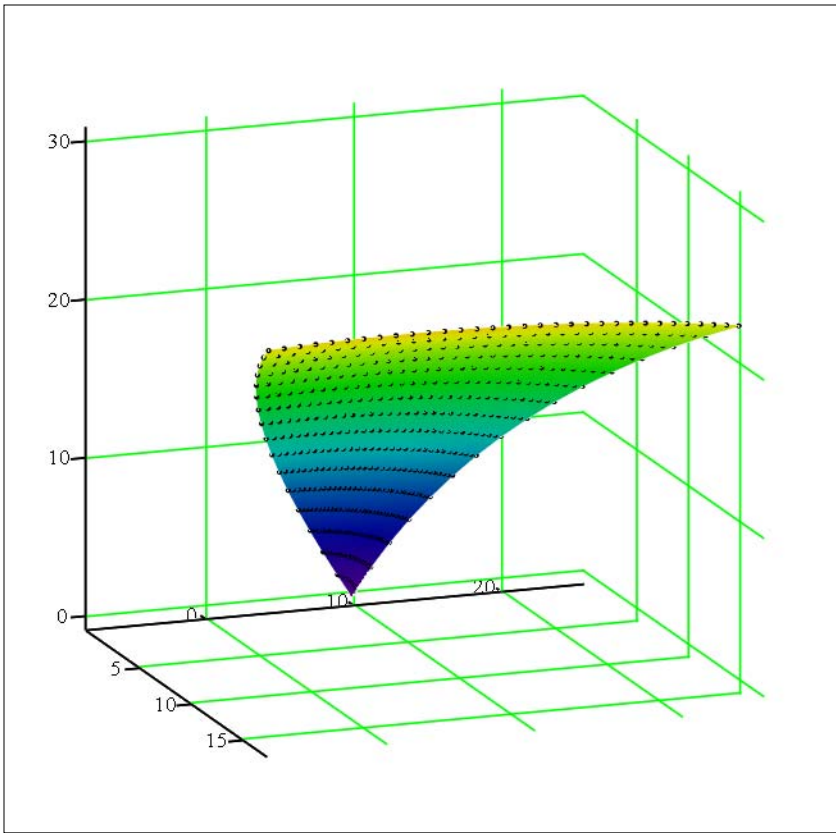
Corriente I_{dc}



$S_{I_{sd}}$

$S_{I_{sq}}$

$S_{I_{dc}}$

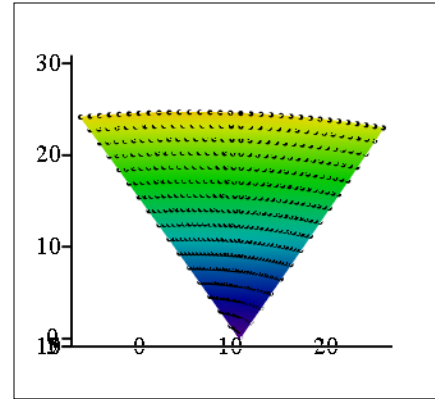


(I_{sd}, I_{sq}, I_{dc})

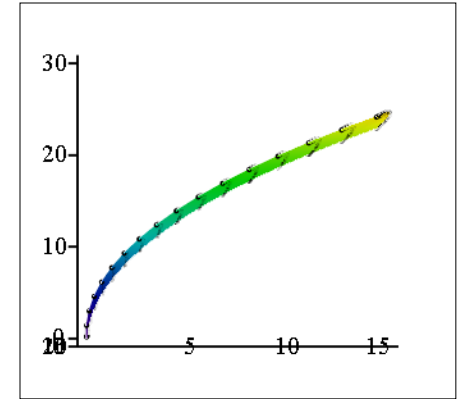
La corriente I_{dc} negativa no es opción, por switches unidireccionales de la topología.

Hay dos entradas M_{rd} y M_{rq} y hay tres variables de estado. Las potenciales salidas podrían ser I_{sd} e I_{sq} , I_{sd} e I_{dc} , I_{dc} e I_{sq} .

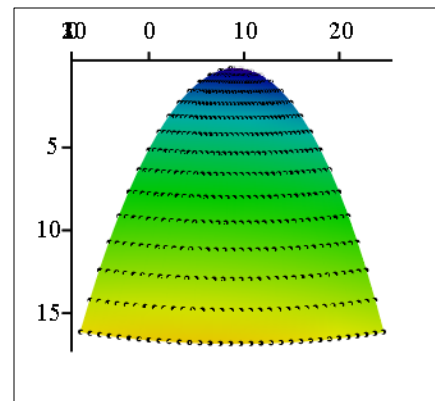
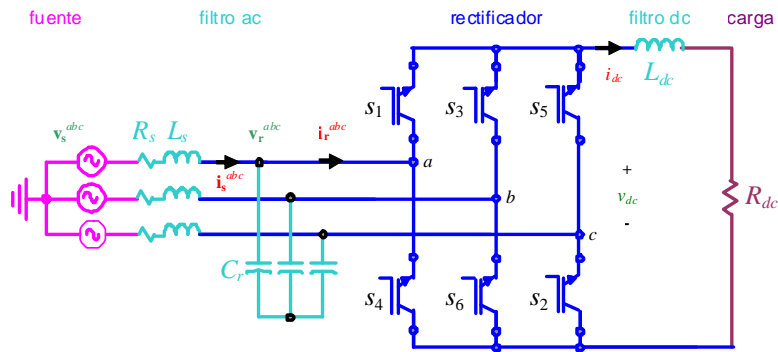
Es posible controlar I_{sd} e I_{sq} , I_{dc} e I_{sq} , pero **NO** se puede controlar I_{sd} e I_{dc} por el rango mínimo.



(I_{sd}, I_{sq}, I_{dc})



(I_{sd}, I_{sq}, I_{dc})



(I_{sd}, I_{sq}, I_{dc})